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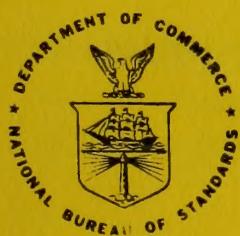
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A New Method of Assigning Uncertainty in Volume Calibration

James A. Lechner, Charles P. Reeve, Clifford H. Spiegelman

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**A NEW METHOD OF ASSIGNING
UNCERTAINTY IN VOLUME CALIBRATION**

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With acknowledged assistance from
John R. Goss and Julie N. Knapp

Issued December 1980

U. S. DEPARTMENT OF COMMERCE, Philip M. Klutznick, Secretary

Jordan J. Baruch, Assistant Secretary for Productivity, Technology, and Innovation

NATIONAL BUREAU OF STANDARDS, Ernest Ambler, Director

THIS PAPER PRESENTS A PRACTICAL COMPUTATIONAL OVERVIEW OF THE VOLUME-
VOLUME CALIBRATION CURVE FOR LARGE-SCALE NUCLEAR WASTEWATER PROCESSING EQUIP-
MENT. IT EXPLAINS THE APPROXIMATIONS OF ASSUMING VOLUME CALIBRATION
POLYNOMIALS TO BE LINEAR, AND THE METHODS OF DETERMINING THE

***A NEW METHOD OF ASSIGNING UNCERTAINTY IN VOLUME CALIBRATION**

by

James A. Lechner
Charles P. Reeve
Clifford H. Spiegelman

with programming assistance from
Martin Ross Cordes and Janice M. Knapp

***Work supported (in part) by the U. S. Nuclear Regulatory Commission.**

ABSTRACT

The direct measurement of liquid volume in large processing tanks. This paper presents a practical statistical overview of the pressure-volume calibration curve for large nuclear materials processing tanks.

It explains the appropriateness of applying splines (piecewise polynomials) to this curve, and it presents an overview of the associated statistical uncertainties. In order to implement these procedures a practical and portable FORTRAN IV program is provided along with its users' manual. Finally, the recommended procedure is demonstrated on actual tank data collected by NBS.

Key Words: Volume calibration; differential pressure; splines; accountability; statistics.

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1. Introduction.

The direct measurement of liquid volume in large processing tanks, especially with internal structure, is impractical at best. Measuring (differential) pressure is simple and quick. However, in order to estimate the volume indirectly by observing pressure, it is necessary to use the relationship between volume and pressure. This relationship is known as a calibration curve; its estimation is the process known as calibration.

Fitting a calibration curve is much like regression, in that for "known" values v_i of volume, one obtains one or more observations p_{ij} of the differential pressure $p_i = p(v_i)$, and "fits" a response function $p(v)$ by statistical methods - usually by least squares. At this point, the correspondence stops. Whereas regression is used to predict values of the dependent variable (p) for given values of the independent variable (v), or to test a proposed relationship between the variables, a calibration curve is used to estimate values of the independent variable v corresponding to new measured values of the dependent variable p . Furthermore, the confidence interval (or uncertainty measure) which is desired is not for p , but rather for v . And finally, systematic error is introduced by lack of fit of the calibration curve, and in a materials accounting situation this may be crucial.

This paper presents a method for producing valid uncertainty limits for the pressure-volume tank calibration curve by using calibration functions which are smooth, piecewise polynomial functions called "splines." Taking advantage of an approach to calibration originated by Scheffé [1] and further elucidated by Scheffé, Rosenblatt and

Spiegelman [2], it provides statistically sound uncertainty limits, not just for a single estimated value of volume, but for all volumes estimated by use of the fitted curve. This approach overcomes a major theoretical problem with earlier methods: it makes proper allowance for the contribution to the overall uncertainty of errors in fitting the curve.

The procedure presented herein has been implemented, based upon a spline-fitting program due to deBoor [3]. The resulting FORTRAN program has been tested on various sets of data, including actual tank data.

The remainder of this paper is organized as follows. Section 2 contains a discussion of the pressure-volume model, and the statistics of calibration. Section 3 contains a discussion of an example, and of the printout produced by the program. Section 4 is essentially a users' manual for the program. In Section 5 will be found a discussion of open questions, work in progress, cautions, and possible extensions of this technique. Finally, Appendix 1 contains a discussion of Scheffe's constant c , used as an input to the program, and Appendix 2 contains a listing of the program.

2. The Scientific Basis for, and Interpretation of, a Calibration Curve.

In order to provide statistically valid uncertainty limits for the volume estimates obtained through the use of a calibration curve, it is necessary to have a prior model for the pressure-volume relationship. That is, while the constants in the model for the relationship may be determined from the data, the form of the model must not depend on the data to be used in fitting the relationship. In addition, the less accurately the hypothesized model describes this relationship, the less

valid will be the resulting uncertainty statements. That is, inaccuracies in the hypothesized model will lead to systematic differences between true and fitted curves. In order to obtain valid uncertainty statements, bounds for such differences must be determined, and added to the statistical uncertainty as systematic error limits.

The interiors of large processing tanks do not generally conform to idealized geometrical shapes, such as cylinders. Often, however, the tank can be considered to be composed only of segments for which an idealized model is a good representation. In this paper it is assumed that the tank is composed of a finite number, $k+1$, of distinct and known regions where the idealized relationship between the two variables pressure, p , and volume, v , is given by

$$\begin{aligned} p &= f(v) \\ &= g_1(v) \quad \xi_0 < v < \xi_1 \\ &= g_2(v) \quad \xi_1 < v < \xi_2 \\ &\vdots \\ &= g_{k+1}(v) \quad \xi_k < v < \xi_{k+1} . \end{aligned}$$

In addition, continuity of the relationship at the interior "knots" ξ_i , $i=1, \dots, k$ is required.

In all that follows, volume and height refer to the portion of the tank above the bottom of the diptube used to measure pressure. The portion of the tank below that point is known as the heel, and is not treated in this paper. The pressure measured is the difference in

pressure between the bottom of the diptube and a reference point at the top of the tank.

The pressure-volume relationship can be ascertained from the following two equations. At height h the volume in the container is

$$v = \int_0^h A(x) dx$$

where $A(x)$ is the cross-sectional area at height x . Also, when the liquid height is h , $p = \rho gh$, where ρ is the density of the homogeneous liquid and g is the acceleration due to gravity. Using these two equations one easily obtains

$$v = \int_0^{p/\rho g} A(x) dx .$$

Thus $\frac{\partial v}{\partial p} = \frac{1}{\rho g} A(p/\rho g)$ and hence in areas of the tank where $A(x)$ is

constant the volume-pressure relationship is a straight line.

If $A(x)$ is constant* in region i , as it obviously is for at least some regions of the tank shown in Figure 1, then

$$(1) \quad p = g_i(v) = \gamma_i + \beta_i v \text{ for } \xi_{i-1} < v < \xi_i, \quad i=1, \dots, k+1.$$

We assume that each pressure measurement has a random error associated with it, and that these errors are independent and

* If $A(x)$ is not constant on an interval, then p is not a linear function of v on that interval. The program under discussion uses the B-spline basis when higher-order polynomial splines are required, because as pointed out in reference [4], the use of simpler representations of polynomial splines may lead to numerical instability.

normally-distributed, with mean zero and constant variance σ^2 . (Recall that volume is assumed to be measured with no significant error.) Because of these errors, only estimates of the coefficients γ_i and β_i are obtained during the calibration process (experiment). These coefficient estimates are then used during plant operation to obtain estimates of the volume in the tank, utilizing the inverse of the relationship (1).

Determination of uncertainty limits on these estimates is not trivial. There are two sources of random error: estimation of the coefficients γ and β in the calibration experiment, and measurement of p during operational use of the tank. The familiar linear regression model has properties, such as the nonexistence of means and variances of reciprocals, which make the analysis difficult. Special justification involving asymptotic (large sample-size) behavior is thus required in order to use a propagation-of-error approach to obtain appropriate approximate uncertainty limits on the estimated volumes. Furthermore, unless the p - v relationship is linear, normally distributed errors in the p -measurements during operation produce non-normal errors in the resulting estimates of v . The usual propagation-of-error technique does not take into account the differing characteristics of these errors. The new technique presented in this paper, in contrast to the propagation-of-error approach just mentioned, does allow a correct accounting for both.

The calibration chart (i.e., the table of uncertainty limits) is produced after choosing two probabilities, α and δ . An exact statement giving the interpretation of these probabilities may be found in Scheffé

[1] and in Scheffé, Rosenblatt, and Spiegelman [2]. However, an expanded, more heuristic explanation is given here. First, we require bounds for the calibration curve which will contain the entire curve with a prechosen probability $1-\delta$. (Thus, δ can be thought of as describing the uncertainty level to be associated with the outcome of the initial calibration experiment.) These bounds guarantee, with probability $1-\delta$, that for any and every future volume v within the range of calibration of the tank, the v -interval (see Figure 2) that would be obtained by projection of the value $f(v)$ through the curves to \underline{v} and \bar{v} would contain v . The second probability level to be chosen is α . (Here α can be thought of as describing the uncertainty level to be attributed to errors in future individual pressure measurements.) If σ were known, we could state that the true pressure $f(v)$ at the unknown volume v lies within the $1-\alpha$ confidence interval $(p - z_{1-\alpha/2}\sigma, p + z_{1-\alpha/2}\sigma)$ with probability $1-\alpha$, where p is the observed pressure and $z_{1-\alpha/2}$ is the two-sided $1-\alpha$ value for a normal distribution. The Scheffé procedure expands this interval appropriately, to account for the facts that σ is estimated and that this estimate is used for the $1-\delta$ bound on the curve and for bounds on many different $f(v)$. It then combines the $1-\alpha$ confidence interval for $f(v)$ with the $1-\delta$ bounds on the calibration curve to produce calibration intervals $I(p)$ for v . Construction of the calibration intervals is shown schematically in Figure 3. A set of intervals $I(p_1)$ for p_1 in the range of values obtained during the calibration experiment is called a calibration chart (see Figure 4).

In the discussion of the example presented in the next section, more detail on the nature of the steps that make up a calibration run will be found.

3. An Example.

This example relates to a processing tank, roughly circular in cross section, but with internal structure consisting of cooling coils, stirrers, braces, etc. [5]. This tank is pictured in Figure 1. The data from calibration runs on this tank have graciously been made available by the author of reference [5].

There were five calibration runs for which the data were useful for this analysis. One run was done in the canyon where the tank is to be used. The other four, done in a mock-up area, used smaller tubing in the pressure-measuring system. This smaller tubing was known to cause systematic differences in the pressure measurement, which were expected to be linearly related to pressure for each run. Since the tubing in the canyon was sufficiently large to render the pressure drop insignificant, the systematic error was estimated for each of the other four runs, and a correction made by applying a linear transformation to the measured pressure. It should be noted that these corrections, made to four of the five runs, effectively decrease the degrees of freedom for the error sum of squares by eight (two correction parameters times four runs corrected).

The calibration program was applied to these data, as were various other techniques available on the large central computer at NBS. The results will now be presented and their use described.

In the version of the program described here, the knot locations are input by the analyst. It is presumed that the knot locations can be adequately prescribed from the blueprints and other knowledge about the tank. (A refinement which allows the automatic determination of the

number and location of knots is being investigated.) The program displays the given knot locations and other input data, as shown in Figure 5. Next come the results of the fitting operation, as shown in part in Figure 6. Note that the fit here is a fit of observed pressure (y) as a function of the accurately-dispensed volume (x); it is pressure which is subject to errors of observation, and volume which is essentially known. The residual standard deviation, an estimate of the standard deviation of the pressure measurements, is derived from the residuals or deviations of the measured pressures from the fitted curve. In this case, its value is 1.49 pascals. This value, the corresponding degrees of freedom, and the coefficients (which are in general not immediately interpretable, since they refer to the so-called B-splines, a representation chosen for computational stability), are part of these results. The calibration intervals for estimation of volume from measured pressure are printed next (see Figure 4). An ordinary polynomial representation and a residual plot are also printed as shown in Figures 7 and 8.

It will be instructive to examine the printout and discuss the approach in more detail, and this will now be done.

As can be seen from Figure 5, the program duplicates the end knots. This is just a simple way to define the B-spline basis functions which are used to perform the fit, and need not concern the analyst. The input values for knot locations, degree of fit, and other miscellaneous parameters are printed out for verification.

At this point, the program does a linear least squares fit of the specified model to the (v, p) data, and prints out a reasonably standard summary (Figure 6). The column labels are self-explanatory. At the bottom of this summary are found the residual standard deviation and its associated degrees of freedom, and the estimated coefficients with the corresponding estimated standard deviations.

The program next computes some intermediate results which generally are of no interest to the analyst, and therefore are only printed out if requested. These are confidence intervals for p , at 300 evenly-spaced points covering the range of v between the extreme knots. Input values of α , δ , and c are used in this procedure, so these values are printed.

The calibration chart comes next, giving the predicted value of v and the corresponding lower and upper limits for each of the specified set of p -values (see Figure 4). It is obtained by inverse interpolation from the confidence intervals for p discussed in the preceding paragraph. Usually, the extreme values of p will be at least partially outside the range of at least one of the curves. When this happens, the intervals should extend either to zero volume or to full volume. This is indicated by "<" and ">" respectively on the printout.

Since the coefficients actually fitted are the B-spline coefficients, the program converts the B-spline representation to a simple polynomial representation. The printout shows the endpoints and the coefficients of the fitted polynomial for each of the specified intervals (see Fig. 7).

Finally, the residuals from the fitted model are plotted in order of increasing volume to allow a visual check of the adequacy of the chosen model [6] (see Fig. 8).

At NBS, with the aid of the central computer and the OMNITAB system [7], a number of other things were tried which strengthen the conviction that this program does indeed work well. These will now be discussed.

Various subsets of the data were fitted to the same model. No inconsistencies were found.

The sensitivity to position and presence of the different knots was checked. The results were rather sensitive to the knot locations, which implies that good estimates of the locations are required for good fits. It should also be noted that where a knot bounds a short segment, the removal of that knot might make very little difference in any global measure of fit quality, unless there are many data points in that short stretch. Nevertheless, the systematic error introduced by deleting that knot can be a consistent source of inventory losses or gains, apparent or real. Thus it is important to include all real segments in the model to be fitted.

A separate program was written to perform linear spline fitting, while the main package was being put together. The answers did not differ between the two programs, providing a partial check that no programming errors were committed.

Smooth higher-order spline fits were tried (quadratic and cubic). There was no improvement in fit. The linear spline appears to provide an adequate representation of the pressure/volume relationship.

Probability plots were done in various ways, looking for possible troubles with the data or the method. Nothing suspicious was found.

4. User's Manual.

This fixed-knot spline package for calibration consists of a "main" subroutine SPLEEN and 29 additional subroutines. The manner in which they interact is diagrammed in Figure 9. All programs are written in FORTRAN and have been checked for portability by the Bell Laboratories PFORT verifier [8]. It was decided that SPLEEN should be a subroutine rather than a main program so that the user could enter the parameter values in the way most convenient for him. The user then must write a main program which sets up the required dimensioned variables and assigns values to the necessary parameters (those with asterisks in the list which follows). These parameters are passed to subroutine SPLEEN via the statement

```
CALL SPLEEN(H,X,Y,W,R1,R2,RES,N,NX,NKX,T,BCOEF,XXI,Q,DIAG,K,  
          KX,YY,NY,NYX,MD,SCRTCH,JX,AL,DL,C,IP)
```

where

- * H(80) = Up to 80 characters in 80A1 format identifying the data
- * X(NX) = Vector (length N) of X-values where observations were made (independent variable)
- * Y(NX) = Vector (length N) of observations
- * W(NX) = Vector (length N) of weights for observations
- R1(NKX) = Vector (length N+K) for scratch area
- R2(NKX) = Vector (length N+K) for scratch area
- RES(NKX) = Vector (length N+K) of residuals from spline fit
- * N = Number of observations
- * NX = Dimension (>N) of vectors X,Y,W
- * NKX = Dimension (>N+K) of vectors R1,R2,RES
- * T(KX) = Vector (length K+2*MD) of knot locations

BCOEF(KX) = Vector (length K+MD-1) of B-spline coefficients
 XXI(KX,KX) = Variance-covariance matrix (size [K+MD-1]×[K+MD-1])
 of B-spline coefficients
 Q(JX,KX) = Matrix (size [MD+1]×[K+MD-1]) for scratch area
 DIAG(KX) = Vector (length K+MD-1) for scratch area

 * K = Number of knots specified by user (later increased to
 K+2*MD by program)

 * KX = Dimension (>K+2*MD) of vectors T, BCOEF, DIAG and
 matrices XXI and Q (column only for Q)

 * YY(NYX) = Vector (length NY) of Y-values for which predicted
 X-values (with confidence intervals) are to be
 computed

 * NY = Number of Y-values for which predicted X-values are
 to be computed

 * NYX = Dimension (>NY) of vector YY

 * MD = Degree of spline (<19); for example, 1=linear,
 2=quadratic, 3=cubic)

 SCRTCH(JX,JX) = Matrix (size [MD+1]×[MD+1]) for scratch area

 * JX = Dimension of square matrix SCRTCH and row dimension
 of matrix Q = 20

 * AL = Alpha level of significance

 * DL = Delta level of significance

 * C = Constant in the interval (0.85,1.25) associated with
 Scheffé's calibration technique (see Appendix 1 for a
 discussion of this constant)

 0 For abbreviated printout
 * IP = 1 For full printout (residuals, PP representation)
 2 For full printout plus Y-confidence intervals for
 300 evenly spaced X-values over knot span

Variables which appear with an asterisk (*) require input values
 from the main program. The subscripts on vectors and matrices
 indicate the dimensions which must be assigned in the main program.

Variable names which begin with the letters I,J,K,L,M, or N are of the INTEGER type. The remaining variable names are of the REAL single precision type.

The print parameter IP gives the user a certain amount of control over the amount of information to be printed out. Normally the most suitable value is IP=1. A value of IP=0 suppresses the printout of the weights, independent variable, observations, predicted values, and residuals. This option may save quite a bit of paper in case there are several hundred observations, but it deprives the user of the chance to visually examine the residuals. A value of IP=2 causes a listing of certain intermediate vectors which are somewhat lengthy and would not normally be of use to the user.

In the interest of minimizing the number of variables needed in the CALL statement, not all of the printed information can be recovered through the passed parameters. Furthermore, three of the variables (X, K, and T) return values different from their input values.

The data points (X_i, Y_i, W_i) may be input in arbitrary order, as may the knot locations T_i and the vector of YY_i specifying the y-values on the calibration chart.

There are two subroutines which check for consistency among the input parameters. Each inconsistency causes a diagnostic message to be printed. If one or more inconsistencies is detected then the program execution is terminated. Observations outside the knot span are flagged and weighted zero. The number of observations is then reduced by one for each flagged point and a diagnostic is printed. This is not a fatal error unless it reduces the number of degrees of freedom to zero or less.

Although this package can handle splines of any degree up to 19 it was primarily intended for splines of lower degree, i.e., linear, quadratic, or cubic. Test runs on sets of both real and artificial data have given valid results up to about degree 9. Beyond that the limitation of single precision arithmetic on the 36-bit NBS central computer begins to cause roundoff errors that invalidate the results. The user should exercise caution when fitting the higher degree splines.

If the user wants to change some of the continuity conditions at a given knot he may do so by duplicating that knot in the knot vector which is passed to subroutine SPLEEN. If a knot appears M times in the fitting of a spline of degree N then the functional value and the first $N-M$ derivatives of the function will be continuous at that knot. If $M = N+1$, neither the function nor its derivatives are required to be continuous.

The package may be applied to both monotone increasing and decreasing calibration curves.

5. Summary and Discussion.

An approach to calibration curves and their uncertainty bands has been presented, complete with a FORTRAN program to perform the required calculations. An example involving a large process tank has been used to illustrate the approach and the program. The results include not only the curve for estimating volume from measured pressure, but also valid uncertainty limits for repeated applications of the calibration curve obtained.

The interval estimates of volume comprise two parts: a long-term component which changes only at recalibration, and a random component.

The contribution due to the long-term component may be estimated in large scale calibration experiments by the volume interval estimate obtained when $\alpha=1$. Similarly, the contribution due to the random component may be estimated by the volume interval estimate obtained when $\delta=1$. When the calibration experiment is of a more modest size involving less than 100 data points the above component estimates may not be realistic. However a more comprehensive treatment for combining interval estimates (and hence their components) obtained from a calibration curve is under development by C. Spiegelman and K. Eberhardt [9].

The results of a calibration will be used repeatedly, usually without any further opportunity to verify their correctness, until the next calibration. Therefore it is important that the measurement system be under control. In the work reported here, the run-to-run differences observed in the mock-up area were due to a known source (the small diameter of the tubing), and could be corrected. If any anomalous behavior is observed which cannot be satisfactorily explained, then of course the entire statistical analysis must be approached with caution.

Little has been written about the design of calibration experiments - i.e., the selection of volumes at which pressure is to be measured, the number of measurements to be taken at each volume, and the arrangement of these measurement points into a sequence of runs. One solution to this question has been achieved by Spiegelman and Studden, and will be published in the NBS Journal of Research [10]. In general, later runs will concentrate on certain sections of a tank, but it is good practice to ensure that at least two runs cover each section, and that several runs cover the whole tank. If this precaution is not taken, there might

be very little cross-validation between runs.

Certain caveats ought to be mentioned here. The program under discussion assumes that the knot locations are known, and that the model is correct. Consequences of failure of these assumptions could be severe. With respect to the knot locations, careful inspection of the residual plots will sometimes indicate discrepancies. These may be small; however, it is important to realize that such regions represent systematic deviations, and could be used (at least in theory) to cover the diversion of material. An approach to the problem involving unknown knot locations is being pursued at this writing.

Unlike a simple linear regression, where the inclusion of a superfluous higher-order term generally causes no major trouble (the fitted coefficient turns out insignificantly small, and the residual mean square increases minimally), choosing a higher-order model when fitting smooth splines can result in a very much worse fit. This is because of the smoothing restrictions, which greatly limit the freedom of the fitting procedure. (Imagine that the true model consists of two straight lines meeting at a point. If one chooses to fit a quadratic spline, then one is insisting on having two quadratic curves which meet at the proper x -value, and which have the same slope at that point. Thus the slope at that point is probably going to be some value between the two straight-line slopes, and the fit cannot be accurate.) One way around this difficulty is to fit piecewise polynomials (i.e., do not require smoothness), and investigate the appropriate degree from these fits. However, it is much better to know the situation well enough to choose the correct model from physical considerations.

A technique that the authors have found useful is to run the program described here with the degree of the fit set equal to zero. The result is to fit a step function to the data, and to produce a plot of the residuals from that fit; for the Example of this paper, that plot is reproduced as Figure 10. It can be seen that the residuals look as linear as a printer plot can look. Therefore, a first-degree (linear) spline fit is the proper choice. If in some segment the relationship were not linear, this plot should show it. The plot also gives some idea of the spread of points across the intervals, though of course near-duplicate points will plot as one because it is a discrete printer plot.

Note that the continuity restrictions can be relaxed when using the program under consideration, by simply duplicating the knots. See Section 4 for details.

Appendix 1.

As stated in Section 4, a constant c must be input by the user. In order to obtain this constant from tables 1 and 2 in Scheffé (1973) for $1 \leq p \leq 10$ the user must have calculated the standard deviation, SD , for $p(v)$ in the complete region of calibration. The smallest and largest values the $SD(p(v))/\sigma$ over the complete calibration region are used as input for the Scheffé tables. For $k > 10$ Scheffé gives a mathematical algorithm for finding c , and states that for very large (asymptotic) values of $n-k$, $c=1$. (Here n is the number of observations, and k is the number of B-spline coefficients.) If the reader does not wish to do a Scheffé table 1 or table 2 lookup, the following table gives approximate and generally larger values for this constant.

Approximate c values for $1 \leq k \leq 10$

$n-k$	60-119	120-149	150 +
c	1.10	1.05	1.00

Appendix 2.

Program Listing.

The subroutines which make up the spline-fitting package follow, in alphabetical order.

```

1      C----- SUBROUTINE ADKNTS ( T, K, KX, MO )
2      C----- ADKNTS
3      C----- WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
4      C----- DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D. C.
5      C----- AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
6      C----- FOR: DUPLICATING THE FIRST AND KTH (LAST) ENTRIES OF THE KNOT
7      C----- VECTOR T (MO-1) TIMES
8      C----- SUBPROGRAMS CALLED: -NONE-
9      C----- CURRENT VERSION COMPLETED OCTOBER 10, 1979
10     C----- ADKNTS01
11     C----- ADKNTS02
12     C----- ADKNTS03
13     C----- ADKNTS04
14     C----- ADKNTS05
15     C----- ADKNTS06
16     C----- ADKNTS07
17     C----- ADKNTS08
18     C----- ADKNTS09
19     C----- ADKNTS10
20     C----- ADKNTS11
21     C----- ADKNTS12
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43     C----- ADKNTS34
44     C----- ADKNTS35
45     C----- ADKNTS36
46     C----- ADKNTS37
47     C----- ADKNTS38
48     C----- ADKNTS39
49     C----- ADKNTS40
50     C----- ADKNTS41
51     C----- ADKNTS42
52     C----- ADKNTS43

1      C----- DIMENSION T(KX)
2      C----- FORMAT (//1X, 29(1H-) /1X, 29H* SUMMARY OF KNOT LOCATIONS * /1X,
3      C----- 2 29(1H-) //5X, 1H1, 6X, 8HKNOTS(1) /)
4      C----- FORMAT (2X, 14, G15.6)
5      C----- FORMAT (/-5X, 30H<<< EACH END KNOT DUPLICATED, I3, 1X,
6      C----- 2 11HTIMES >>>)
7      C----- SAVE END KNOT LOCATIONS
8      C----- Q1=T(1)
9      C----- Q2=T(K)
10     C----- INCREASE INDEX OF EACH KNOT LOCATION BY (MO-1)
11     C----- KM=K+MO
12     DO 40 I=1, K
13     KM1=KM-1
14     KI=K-1+1
15     T(KM1)=T(KI)
16     CONTINUE
17     ADD DUPLICATE END KNOT LOCATIONS AT THEIR RESPECTIVE ENDS
18     MD=MO-1
19     DO 50 I=1, MD
20     KM1=KM+I-1
21     T(I)=Q1
22     T(KM1)=Q2
23     CONTINUE
24     RECOMPUTE THE LENGTH OF THE VECTOR T
25     K=K+2*MD
26     WRITE (6,30) MD
27     C----- WRITE NEW VECTOR OF KNOT LOCATIONS
28     WRITE (6,10)
29     DO 60 I=1, K
30     WRITE (6,20) I, T(I)
31     CONTINUE
32     RETURN
33
34
35
36
37
38
39
40
41
42
43

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1  CPR*NS( 1 ) .BCHFAC( 2 ) SUBROUTINE BCHFAC ( W, NBNMX, NBANDS, NROW, DIAG )
2  C  FROM * A PRACTICAL GUIDE TO SPLINES * BY C. DE BOOR
3  C  CONSTRUCTS CHOLESKY FACTORIZATION
4  C  C = L * D * L-TRANSPOSE
5  C  WITH L UNIT LOWER TRIANGULAR AND D DIAGONAL, FOR GIVEN MATRIX C OF
6  C  ORDER NROW ; IN CASE C IS (SYMMETRIC) POSITIVE SEMIDEFINITE
7  C  AND B AND D , HAVING N BANDS DIAGONALS AT AND BELOW THE
8  C  MAIN DIAGONAL.
9  C
10 C***** I N P U T *****
11 C NROW... IS THE ORDER OF THE MATRIX C .
12 C NBNMX... THE ACTUAL ROW DIMENSION OF W.
13 C NBANDS... INDICATES ITS BANDWIDTH.
14 C C( I, J ) = 0 FOR ABS( I-J ) .GT. NBANDS .
15 C W.... WORKARRAY OF SIZE (NBANDS, NROW) CONTAINING THE NBANDS DIAGO-BCHFAC15
16 C NALS IN ITS ROWS, WITH THE MAIN DIAGONAL IN ROW 1 . PRECISELY, BCHFAC16
17 C W( I, J ) CONTAINS C( I+J-1, J ) , I=1,...,NBANDS, J=1,...,NROW.
18 C FOR EXAMPLE, THE INTERESTING ENTRIES OF A SEVEN DIAGONAL SYM-BCHFAC18
19 C METRIC MATRIX C OF ORDER 9 WOULD BE STORED IN W AS BCHFAC19
20 C
21 C 11 22 33 44 55 66 77 88 99
22 C 21 32 43 54 65 76 87 98
23 C 31 42 53 64 75 86 97
24 C 41 52 63 74 85 96
25 C
26 C ALL OTHER ENTRIES OF W NOT IDENTIFIED IN THIS WAY WITH AN EN-BCHFAC26
27 C TRY OF C ARE NEVER REFERENCED .
28 C DIAG... IS A WORK ARRAY OF LENGTH NROW .
29 C
30 C***** O U T P U T *****
31 C W.... CONTAINS THE CHOLESKY FACTORIZATION C = L*D*L-TRANS, WITH
32 C W( I, I ) CONTAINING L*D( I, I )
33 C AND W( I, J ) CONTAINING L( I-1+J, J ) , I=2,...,NBANDS.
34 C
35 C***** M E T H O D *****
36 C GAUSS ELIMINATION, ADAPTED TO THE SYMMETRY AND BANDEDNESS OF C .
37 C USED .
38 C NEAR ZERO PIVOTS ARE HANDLED IN A SPECIAL WAY. THE DIAGONAL ELEMENT G( N, N ) = W( 1, N ) IS SAVED INITIALLY IN DIAG( N ), ALL N. AT THE N-BCHFAC39
39 C TH ELIMINATION STEP, THE CURRENT PIVOT ELEMENT, VIZ. W( 1, N ) , IS COMPARED WITH ITS ORIGINAL VALUE, DIAG( N ) . IF, AS THE RESULT OF PRIOR
40 C ELIMINATION STEPS, THIS ELEMENT HAS BEEN REDUCED BY ABOUT A WORD LENGTH, ( I.E., IF W( 1, N )+DIAG( N ) .LE. DIAG( N ) ), THEN THE PIVOT IS DE-BCHFAC42
41 C CLARED TO BE ZERO, AND THE ENTIRE N-TH ROW IS DECLARED TO BE LINEARLYBCHFAC44
42 C DEPENDENT ON THE PRECEDING ROWS. THIS HAS THE EFFECT OF PRODUCING BCFAC45
43 C X( N ) = 0 WHEN SOLVING C*X = B FOR X, REGARDLESS OF B. JUSTIFIC-BCHFAC46
44 C ATION FOR THIS IS AS FOLLOWS. IN CONTEMPLATED APPLICATIONS OF THIS BCFAC47
45 C PROGRAM, THE GIVEN EQUATIONS ARE THE NORMAL EQUATIONS FOR SOME LEAST-BCHFAC48
46 C SQUARES APPROXIMATION PROBLEM, DIAG( N ) = C( N, N ) GIVES THE NORM-SQUAREBCHFAC49
47 C OF THE N-TH BASIS FUNCTION, AND, AT THIS POINT, W( 1, N ) CONTAINS THEBCHFAC50
48 C NORM-SQUARE OF THE ERROR IN THE LEAST-SQUARES APPROXIMATION TO THE N-BCHFAC51
49 C TH BASIS FUNCTION BY LINEAR COMBINATIONS OF THE FIRST N-1 . HAVING BCFAC52
50 C W( 1, N )+DIAG( N ) .LE. DIAG( N ) SIGNIFIES THAT THE N-TH FUNCTION IS LIN-ECHFAC53
51 C EARLY DEPENDENT TO MACHINE ACCURACY ON THE FIRST N-1 FUNCTIONS, THEREBCHFAC54
52 C BEFORE CAN SAFELY BE LEFT OUT FROM THE BASIS OF APPROXIMATING FUNCTIONSBCHFAC55
53 C BCFAC56
54 C BCFAC57
55 C
56 C THE SOLUTION OF A LINEAR SYSTEM
57 C

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58      C IS EFFECTED BY THE SUCCESSION OF THE FOLLOWING TWO CALLS:      BCHFAC58
59      C CALL BCHFAC (W, NBNDMX, NBANDS, NROW, DIAG) : TO GET FACTORIZATION      BCHFAC59
60      C CALL BCHSLV (W, NBNDMX, NBANDS, NROW, DIAG) : TO SOLVE FOR X.      BCHFAC60
61      C THE VECTOR B NOW CONTAINS X.      BCHFAC61
62      C MODIFICATION BY.      BCHFAC62
63      C
64      C MARTIN CORDES      BCHFAC63
65      C CENTER FOR APPLIED MATHEMATICS, MBS      BCHFAC64
66      C VERSION 1      BCHFAC65
67      C OCT 1979      BCHFAC66
68      C
69      C
70      C-----+
71      INTEGER NBNDMX, NBANDS, NROW, I, JMAX, J, JMAX, N      BCHFAC71
72      REAL W(NBNDMX, NROW), DIAG(NROW), RATIO      BCHFAC72
73      IF (NROW.GT.1) GO TO 10      BCHFAC73
74      IF (W(1,1).GT.0.) W(1,1)=1./W(1,1)      BCHFAC74
75      RETURN      BCHFAC75
76      STORE DIAGONAL OF C IN DIAG.      BCHFAC76
77      DO 20 N=1, NROW      BCHFAC77
78      DIAG(N)=W(1,N)      BCHFAC78
79      C
80      DO 79 N=1, NROW      FACTORIZATION      BCHFAC79
81      IF (W(1,N)+DIAG(N).GT. DIAG(N)) GO TO 40      BCHFAC80
82      DO 30 J=1, NBANDS      BCHFAC81
83      W(J,N)=0.      BCHFAC82
84      GO TO 79      BCHFAC83
85      40      W(1,N)=1./W(1,N)      BCHFAC84
86      IMAX=MIN(NBANDS-1, NROW-N)      BCHFAC85
87      IF (IMAX.LT. 1) GO TO 79      BCHFAC86
88      JMAX=IMAX      BCHFAC87
89      DO 60 I=1, IMAX      BCHFAC88
90      RATIO=W(I+1,N)*W(1,N)      BCHFAC89
91      DO 50 J=1, JMAX      BCHFAC90
92      L1=N+1      BCHFAC91
93      L2=J+1      BCHFAC92
94      W(J,L1)=W(J,L1)-W(L2,N)*RATIO      BCHFAC93
95      JMAX=JMAX-1      BCHFAC94
96      W(I+1,N)=RATIO      BCHFAC95
97      CONTINUE      BCHFAC96
98      RETURN      BCHFAC97
99      END      BCHFAC98

```

CPR*N(S(1).BCHSLV(1))

```

1      SUBROUTINE BCHSLV (W,NBNDMX,NBANDS,NROW,B)
2      C  FROM * A PRACTICAL GUIDE TO SPLINES *  BY C. DE BOOR
3      C  SOLVES THE LINEAR SYSTEM C*X = B  OF ORDER N R O W  FOR  X
4      C  PROVIDED W CONTAINS THE CHOLESKY FACTORIZATION FOR THE BANDED (SYM-
5      C  METRIC) POSITIVE DEFINITE MATRIX C AS CONSTRUCTED IN THE SUBROUTINE BCHSLV05
6      C  B C H F A C (QUO VIDE).
7
8      C***** I N P U T *****
9      C  NROW....IS THE ORDER OF THE MATRIX C .
10     C  NBNDMX....THE ACTUAL ROW DIMENSION OF W.
11     C  NBANDS....INDICATES THE BANDWIDTH OF C .
12     C  W....CONTAINS THE CHOLESKY FACTORIZATION FOR C , AS OUTPUT FROM
13     C  SUBROUTINE BCHFAC (QUO VIDE).
14     C  B....THE VECTOR OF LENGTH N R O W  CONTAINING THE RIGHT SIDE.
15
16     C***** O U T P U T *****
17     C  B....THE VECTOR OF LENGTH N R O W  CONTAINING THE SOLUTION.
18
19     C***** M E T H O D *****
20     C  WITH THE FACTORIZATION C = L*D*L-TRANSPOSE  AVAILABLE, WHERE L  IS
21     C  UNIT LOWER TRIANGULAR AND D  IS DIAGONAL, THE TRIANGULAR SYSTEM
22     C  L*Y = B  IS SOLVED FOR Y (FORWARD SUBSTITUTION). Y IS STORED IN B,
23     C  THE VECTOR D**(-1)*Y IS COMPUTED AND STORED IN B, THEN THE TRIANG-
24     C ULAR SYSTEM L-TRANSPOSE*X = D**(-1)*Y IS SOLVED FOR X (BACKSUBSTITUTION).
25
26     C  MODIFICATION BY.
27
28     C
29     C  MARTIN CORDES
30     C  CENTER FOR APPLIED MATHEMATICS, MBS
31     C  VERSION 1
32     C  OCT 1979
33
34
35
36     INTEGER NBNDMX,NBANDS,NROW,J,JMAX,N,NBNDM1
37     REAL W(NBNDMX,NROW),B(NROW)
38     IF (NROW.GT.1) GO TO 10
39     B(1)=B(1)*W(1,1)
40     RETURN
41
42     C  FORWARD SUBSTITUTION. SOLVE L*Y = B FOR Y, STORE IN B.
43     C  NBNDM1=NBANDS-1
44     DO 30 N=1,NROW
45     JMAX=MIN0(NBNDM1,NROW-N)
46     IF (JMAX.LT.1) GO TO 30
47     DO 20 J=1,JMAX
48     L=J+N
49     B(L)=B(L)-W(J+1,N)*B(N)
50     CONTINUE
51
52     C  BACKSUBSTITUTION. SOLVE L-TRANSF.X = D**(-1)*Y  FOR X, STORE IN B.
53     N=NROW
54     B(N)=B(N)*W(1,N)
55     JMAX=MIN0(NBNDM1,NROW-N)
56     IF (JMAX.LT.1) GO TO 60
57     DO 50 J=1,JMAX

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```

58      L=J+N
59      B(N)=B(N)-W(J+1,N)*B(L)
60      N=N-1
61      IF (N,GT,0) GO TO 40
62      RETURN
63      END

```

BCHSLV58
BCHSLV59
BCHSLV60
BCHSLV61
BCHSLV62
BCHSLV63

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1      .1. BSPLPP(1)      .2. BSPLPP(1)
1      SUBROUTINE BSPLPP (T, BCOEF, N, K, SCRATCH, BREAK, COEF, L, KMAX)
2      C FROM * A PRACTICAL GUIDE TO SPLINES * BY C. DE BOOR
3      CALLS BSPLVB
4      C CONVERTS THE B-REPRESENTATION T, BCOEF, N, K OF SOME SPLINE INTO ITS
5      C PP-REPRESENTATION BREAK, COEF, L, K .
6
7      C*****
8      C   I N P U T *****
9      C   T.....KNOT SEQUENCE, OF LENGTH N+K
10     C   BCOEF....B-SPLINE COEFFICIENT SEQUENCE, OF LENGTH N
11     C   N.....LENGTH OF BCOEF AND DIMENSION OF SPLINE SPACE
12     C   K.....ORDER OF THE SPLINE
13     C   KMAX.....ROW DIMENSION OF ARRAYS COEF AND SCRATCH
14     C
15     C   W A R N I N G . THE RESTRICTION K .LE. KMAX (= 20) IS IMPO-
16     C   SED BY THE ARBITRARY DIMENSION STATEMENT FOR BIATX BELOW. BUTBSPLP016
17     C   IS N O W H E R E C H E C K E D FOR.
18     C
19     C*****
20     C   S C R A T C H . . . . . O F S I Z E (KMAX, K) ' N E E D E D T O C O N T A I N B C O E F F S O F A P I E C E
21     C   O F T H E S P L I N E A N D I T S K-1 D E R I V A T I V E S
22     C
23     C*****
24     C   O U T P U T *****
25     C   B R E A K . . . . . B R E A K P O I N T S E Q U E N C E , O F L E N G T H L+1, C O N T A I N S ( I N I N C R E A S-
26     C   I N G O R D E R ) T H E D I S T I N C T P O I N T S I N T H E S E Q U E N C E T(K0, . . . , T(N+1) ) B S P L P 0 2 5
27     C   C O E F . . . . . A R R A Y O F S I Z E ( K M A X , N ) , W I T H C O E F ( I , J ) = ( I-1) S T D E R I V A T I V E
28     C   O F S P L I N E A T B R E A K ( J ) F R O M T H E R I G H T
29     C   L . . . . . N U M B E R O F P O L Y N O M I A L P I E C E S W H I C H M A K E U P T H E S P L I N E I N T H E I N-B S P L P 0 2 8
29     C   T E R V A L ( T(K0) , T(N+1) ) , B S P L P 0 2 9
30     C
31     C*****
31     C   M E T H O D *****
32     C   F O R E A C H B R E A K P O I N T I N T E R V A L , T H E K R E L E V A N T B-C O E F F S O F T H E
33     C   S P L I N E A R E F O U N D A N D T H E N D I F F E R E N C E D R E P E A T E D L Y T O G E T T H E B-C O E F F S B S P L P 0 3 3
34     C   O F A L L T H E D E R I V A T I V E S O F T H E S P L I N E O N T H A T I N T E R V A L . T H E S P L I N E A N D B S P L P 0 3 4
35     C   I T S F I R S T K-1 D E R I V A T I V E S A R E T H E N E V A L U A T E D A T T H E L E F T E N D P O I N T B S P L P 0 3 5
36     C   O F T H A T I N T E R V A L , U S I N G B S P L V B R E P E A T E D L Y T O O B T A I N T H E V A L U E S O F B S P L P 0 3 6
37     C   A L L B-S P L I N E S O F T H E A P P R O P R I A T E O R D E R A T T H A T P O I N T .
38     C
38     C   P A R A M E T E R K M A X = 20
39     C
40     C   M O D I F I C A T I O N B Y .
41     C
42     C
43     C   M A R T I N C O R D E S
44     C   C E N T E R F O R A P P L I E D M A T H E M A T I C S , N B S
45     C   V E R S I O N 1
46     C   M A R 1980
47     C
48     C
49     C
50     C   I N T E G E R K, L, N, I, J, J P 1, K M J, L E F T, L S O F A R
51     C   R E A L B C O E F ( 1 ) , C O E F ( K M X , 1 ) , T ( 1 ) , S C R T C H ( K M X , K ) , B I A T X ( 2 0 ) ,
52     C   2 D I F F , F K M J , S U M
53     C   *
54     C   D I M E N S I O N B R E A K ( L+1 ) , C O E F ( K , L ) , T ( N+K ) , D I F F , F K M J , S U M B S P L P 0 5 3
54     C   C U R R E N T F O R T R A N S T A N D A R D M A K E S I T I M P O S S I B L E T O S P E C I F Y T H E L E N G T H O F
55     C   B R E A K , C O E F A N D T P R E C I S E L Y W I T H O U T T H E I N T R O D U C T I O N O F O T H E R W I S E B S P L P 0 5 5
56     C   S U P E R F L U O U S A D D I T I O N A L A R G U M E N T S .
57     C

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58      LSOFAR=0
59      BREAK(1)=T(K)
60      DO 60 LEFT=K, N
61      C           FIND THE NEXT NONTRIVIAL KNOT INTERVAL. GO TO 60
62      IF (T(LEFT+1).EQ.T(LEFT)) GO TO 60
63      LSOFAR=LSOFAR+1
64      BREAK(LSOFAR+1)=T(LEFT+1)
65      IF (K.GT.1) GO TO 10
66      COEF(1,LSOFAR)=BCOEF(LEFT)
67      GO TO 60
68      C           STORE THE K B-SPLINE COEFF. S RELEVANT TO CURRENT KNOT INTERVAL
69      C           IN SCRATCH(.,1).
70      DO 20 I=1,K
71      M=LEFT-K+1
72      SCRATCH(1,1)=BCOEF(MD)
73      C           FOR J=1, . . . , K-1, COMPUTE THE K-J B-SPLINE COEFF. S RELEVANT TO CURRENT KNOT INTERVAL FOR THE J-TH DERIVATIVE BY DIFFERENCING THOSE FOR THE (J-1)ST DERIVATIVE, AND STORE IN SCRATCH(.,J+1).
74      C           FOR J=1, . . . , K-1
75      C           CURRENT KNOT INTERVAL
76      C           DO 30 JP1=2,K
77      C           J=JP1-1
78      C           KMJ=K-J
79      C           KMJ=FLOAT(KMJ)
80      C           DO 30 I=1,KLJ
81      C           M1=LEFT+I
82      C           M2=M1-KMJ
83      C           DIFF=T(M1)-T(M2)
84      C           IF (DIFF.GT.0.) SCRATCH(I,JP1)=((SCRATCH(I+1,J)-SCRATCH(I,J))/DIFF)*FBSPLP085
85      C           2KMJ
86      C           CONTINUE
87      C
88      C           FOR J = 0, . . . , K-1, FIND THE VALUES AT T(LEFT) OF THE J+1 B-SPLINES OF ORDER J+1 WHOSE SUPPORT CONTAINS THE CURRENT KNOT INTERVAL FROM THOSE OF ORDER J (IN BIATX), THEN COMBINE WITH THE B-SPLINE COEFF. S (IN SCRATCH(.,K-J)) FOUND EARLIERBSPLP092 TO COMPUTE THE (K-J-1)ST DERIVATIVE AT T(LEFT) OF THE GIVEN SPLINE.
89      C           NOTE. IF THE REPEATED CALLS TO BSPLVB ARE THOUGHT TO GIVE-BSPLP095 RATE TOO MUCH OVERHEAD, THEN REPLACE THE FIRST CALL BY
90      C           BIATX(1) = 1.
91      C           AND THE SUBSEQUENT CALL BY THE STATEMENT
92      C           J = JP1 - 1
93      C           FOLLOWED BY A DIRECT COPY OF THE LINES
94      C           DELTAR(J) = T(LEFT+J) - X
95      C           BIATX(J+1) = SAVED
96      C           FROM BSPLVB . DELTAL(KMAX) AND DELTAR(KMAX) WOULD HAVE TO
97      C           APPEAR IN A DIMENSION STATEMENT, OF COURSE.
98      C
99      C           CALL BSPLVB (T, 1, 1, T(LEFT), LEFT, BIATX)
100     C           COEF(K,LSOFAR)=SCRATCH(1,K)
101     C           DO 50 JP1=2,K
102     C           CALL BSPLVB (T,JP1,2,T(LEFT),LEFT,BIATX)
103     C           KMJ=K+1-JP1
104     C           SUM=0.
105     C           DO 40 I=1,JP1
106     C           SUM=BIATX(I)*SCRATCH(I,KMJ)+SUM
107     C           COEF(KML,LSOFAR)=SUM
108     C
109     C
110     C
111     C
112     C
113     C
114     C
115     C

```

BSPLP116
BSPLP117
BSPLP117
BSPLP118
BSPLP119

CONTINUE
L=LSOFAR
RETURN
END

116 60
117
118
119

```

CPRNS(1) .BSPLVB(1)
1      SUBROUTINE BSPLVB (T,JHIGH,INDEX,X,LEFT,BIATX)
2      C  FROM * A PRACTICAL GUIDE TO SPLINES * BY C. DE BOOR
3      C  CALCULATES THE VALUE OF ALL POSSIBLY NONZERO B-SPLINES AT X OF ORDER
4      C
5      C      JOUT = MAX( JHIGH , (J+1)*(INDEX-1) )
6      C
7      C      WITH KNOT SEQUENCE T .
8
9      C*****  IN PUT *****
10     C      T,...KNOT SEQUENCE, OF LENGTH LEFT + JOUT , ASSUMED TO BE NONDE-
11     C      GREASING. AS SUMPTION .LT. T(LEFT + 1)
12     C      D I V I S I O N B Y Z E R O WILL RESULT IF T(LEFT) = T(LEFT+1)
13     C      JHIGH,
14     C      INDEX. . . . . INTEGERS WHICH DETERMINE THE ORDER JOUT = MAX(JHIGH,
15     C      (J+1)*(INDEX-1)) OF THE B-SPLINES WHOSE VALUES AT X ARE TO
16     C      BE RETURNED. INDEX IS USED TO AVOID RECALCULATIONS WHEN SEVERAL
17     C      COLUMNS OF THE TRIANGULAR ARRAY OF B-SPLINE VALUES ARE NEEDED (E.G.,
18     C      IN BVALUE OR IN BSPLVD) . PRECISELY,
19     C
20     C      IF INDEX = 1,
21     C      THE CALCULATION STARTS FROM SCRATCH AND THE ENTIRE TRIANGULAR
22     C      ARRAY OF B-SPLINE VALUES OF ORDERS 1,2,...,JHIGH IS GENERATED
23     C      ORDER BY ORDER . I.E., COLUMN BY COLUMN .
24     C      IF INDEX = 2 ,
25     C      ONLY THE B-SPLINE VALUES OF ORDER J+1, J+2, . . . , JOUT ARE GENERATED,
26     C      THE ASSUMPTION BEING THAT BIATX , J , DELTAJ , DELTARBSPLVB25
27     C      ARE, ON ENTRY, AS THEY WERE ON EXIT AT THE PREVIOUS CALL.
28     C      IN PARTICULAR, IF JHIGH = 0, THEN JOUT = J+1, I.E., JUST
29     C      THE NEXT COLUMN OF B-SPLINE VALUES IS GENERATED.
30
31     C      W A R N I N G . . . THE RESTRICTION JOUT .LE. JMAX (= 20) IS IM-
32     C      POSED ARBITRARILY BY THE DIMENSION STATEMENT FOR DELTAJ AND
33     C      DELTARBSPLVB26
34     C      BELOW, BUT IS NOWHERE CHECKED FOR .
35     C
36     C      X. . . . . THE POINT AT WHICH THE B-SPLINES ARE TO BE EVALUATED.
37     C      LEFT. . . . .AN INTEGER CHOSEN (USUALLY) SO THAT
38     C      T(LEFT) .LE. X .LE. T(LEFT+1) .
39
40     C*****  OUT PUT *****
41     C      BIATX. . . . . ARRAY OF LENGTH JOUT , WITH BIATX(J) CONTAINING THE VAL-
42     C      UE AT X OF THE POLYNOMIAL OF ORDER JOUT WHICH AGREES WITH
43     C      THE B-SPLINE B(LEFT-JOUT+1,JOUT,T) ON THE INTERVAL (T(LEFT),
44     C      T(LEFT+1)) .
45     C*****  M E T H O D *****
46     C      THE RECURRENCE RELATION
47
48     C      B( I , J+1 ) (X) = 
$$\frac{X - T(I)}{T(I+J) - T(I)} B(I,J)(X) + \frac{T(I+J+1) - X}{T(I+J+1) - T(I+1)} B(I+1,J)(X)$$

49
50
51
52     C      IS USED (REPEATEDLY) TO GENERATE THE (J+1)-VECTOR B(LEFT-J, J+1)(X) ,
53     C      . . . B(LEFT-J+1)(X) FROM THE J-VECTOR B(LEFT-J+1,J)(X) ,
54     C      B(LEFT,J)(X) , STORING THE NEW VALUES IN BIATX OVER THE OLD. THE
55     C      FACTS THAT
56     C      B(I,1) = 1 IF T(I) .LE. X .LT. T(I+1)
57     C      AND THAT

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58      C      B(I,J)(X) = 0 UNLESS T(I) .LE. X .LT. T(I+J)          BSPLVB58
59      C      ARE USED. THE PARTICULAR ORGANIZATION OF THE CALCULATIONS FOLLOWS AL-BSPLVB59
60      C      ALGORITHM (8) IN CHAPTER X OF THE TEXT.          BSPLVB60
61      C
62      C      PARAMETER JMAX = 20          BSPLVB61
63      C      INTEGER INDEX, JHIGH, LEFT, I, J, JP1          BSPLVB62
64      C      REAL BIATX(JHIGH), T(I), X, DELTAL(JMAX), DELTAR(JMAX), SAVED, TERM          BSPLVB63
65      C      REAL BIATX(JHIGH), T(I), X, DELTAL(20), DELTAR(20), SAVED, TERM          BSPLVB64
66      C      DIMENSION BIATX(JOUT), T(LEFT+JOUT)          BSPLVB65
67      C      CURRENT FORTRAN STANDARD MAKES IT IMPOSSIBLE TO SPECIFY THE LENGTH OF          BSPLVB66
68      C      T AND OF BIATX PRECISELY WITHOUT THE INTRODUCTION OF OTHERWISE          BSPLVB67
69      C      SUPERFLUOUS ADDITIONAL ARGUMENTS.          BSPLVB68
70      C      DATA J /1/          BSPLVB69
71      C      SAVE J, DELTAL, DELTAR (VALID IN FORTRAN 77)          BSPLVB70
72      C
73      C      GO TO (10,20), INDEX          BSPLVB71
74      10      J=1          BSPLVB72
75      C      BIATX(I)=1.          BSPLVB73
76      C      IF (J.GE.JHIGH) GO TO 40          BSPLVB74
77      C
78      20      JP1=J+1          BSPLVB75
79      C      L=LEFT+J          BSPLVB76
80      C      DELTAR(J)=T(L)-X          BSPLVB77
81      C      L=LEFT+1-J          BSPLVB78
82      C      DELTAL(J)=X-T(L)          BSPLVB79
83      C      SAVED=0.          BSPLVB80
84      C      DO 30 I=1,J          BSPLVB81
85      C      L=JP1-1          BSPLVB82
86      C      TERM=BIATX(I)*(DELTAR(I)+DELTAL(L))          BSPLVB83
87      C      BIATX(I)=SAVED+DELTAR(I)*TERM          BSPLVB84
88      C      SAVED=DELTAL(L)*TERM          BSPLVB85
89      C      BIATX(JP1)=SAVED          BSPLVB86
90      C      J=JP1          BSPLVB87
91      C      IF (J.LT.JHIGH) GO TO 20          BSPLVB88
92      C
93      40      RETURN          BSPLVB89
94

```

```

1 CPR*NS(1).BVALUE(2)
2   REAL FUNCTION BVALUE(T,BCOEF,N,K,X,JDERIV)
3   C FROM * A PRACTICAL GUIDE TO SPLINES * BY C. DE BOOR
4   C CALLS INTERV
5   C CALCULATES VALUE AT X OF JDERIV-TH DERIVATIVE OF SPLINE FROM B-REPR.
6   C THE SPLINE IS TAKEN TO BE CONTINUOUS FROM THE RIGHT.
7   C
8   C***** I N P U T *****
9   C T, BCOEF, N, K,... FORMS THE B-REPRESENTATION OF THE SPLINE F TO
10  C BE EVALUATED. SPECIFICALLY,
11  C T...KNOT SEQUENCE, OF LENGTH N+K, ASSUMED NONDECREASING.
12  C BCOEF...B-COEFFICIENT SEQUENCE, OF LENGTH N.
13  C N....LENGTH OF BCOEF AND DIMENSION OF SPLINE(K,T),
14  C A S S U M E D POSITIVE.
15  C K....ORDER OF THE SPLINE .
16  C
17  C W A R N I N G . . . THE RESTRICTION K .LE. KMAX (=20) IS IMPOSED
18  C ARBITRARILY BY THE DIMENSION STATEMENT FOR AJ, DL, DR BELOW,
19  C BUT IS N O W H E R E C H E C K E D FOR.
20  C
21  C X. . . . THE POINT AT WHICH TO EVALUATE
22  C JDERIV. . . . INTEGER GIVING THE ORDER OF THE DERIVATIVE TO BE EVALUATED
23  C A S S U M E D TO BE ZERO OR POSITIVE.
24  C
25  C***** O U T P U T *****
26  C BVALUE. . . . THE VALUE OF THE (JDERIV)-TH DERIVATIVE OF F AT X .
27  C
28  C***** M E T H O D *****
29  C THE NONTRIVIAL KNOT INTERVAL (T(I),T(I+1)) CONTAINING X IS LO-BVALU029
30  C CATED WITH THE AID OF INTERV . THE K B-COEFFS OF F RELEVANT FOR BVALU039
31  C THIS INTERVAL ARE THEN OBTAINED FROM BCOEF (OR TAKEN TO BE ZERO IF BVALU031
32  C NOT EXPLICITLY AVAILABLE) AND ARE THEN DIFFERENCED JDERIV TIMES TO
33  C OBTAIN THE B-COEFFS OF (D**JDERIV)F RELEVANT FOR THAT INTERVAL.
34  C PRECISELY, WITH J = JDERIV, WE HAVE FROM X.(12) OF THE TEXT THAT
35  C
36  C (D**J)F = SUM ( BCOEF(.,J)*B(.,K-J,T) )
37  C WHERE
38  C
39  C   / BCOEF( . ), , , J .EQ. 0
40  C
41  C BCOEF( .,J) = / BCOEF( .,J-1) - BCOEF( .-1,J-1)
42  C   / (T( .+K-J) - T( . ))/(K-J) , J .GT. 0
43  C
44  C
45  C THEN, WE USE REPEATEDLY THE FACT THAT
46  C
47  C SUM ( A( . )*B( .,M,T)(X) ) = SUM ( A( .,X)*B( .,M-1,T)(X) )
48  C WITH
49  C   (X - T( . ))*A( . ) + (T( .+M-1) - X)*A( .-1 )
50  C A( .,X) = (X - T( . )) + (T( .+M-1) - X)
51  C
52  C TO WRITE (D**J)F(X) EVENTUALLY AS A LINEAR COMBINATION OF B- SPLINES BVALU053
53  C OF ORDER 1, AND THE COEFFICIENT FOR B(1,1,T)(X) MUST THEN BE THE BVALU054
54  C DESIRED NUMBER (D**J)F(X). (SEE X.(17)-(19) OF TEXT).
55  C
56  C PARAMETER KMAX = 20
57  C

```

```

58      INTEGER JDERIV, K, N, I, ILO, IMK, J, JC, JCMIN, JCMAX, JJ, KMJ, KM1, MFLAG, NMIBVALU0658
59      2, JDRVPI
60      REAL BCOEF(N), T(1), X, AJ(20), DL(20), DR(20), FKMJ
61      REAL BCOEF(N), T(1), X, AJ(KMAX), DL(KMAX), DR(KMAX), FKMJ
62      C DIMENSION T(N+K)
63      C CURRENT FORTRAN STANDARD MAKES IT IMPOSSIBLE TO SPECIFY THE LENGTH OF TBVALU0663
64      C PRECISELY WITHOUT THE INTRODUCTION OF OTHERWISE SUPERFLUOUS ADDITION-BVALU0664
65      C AL ARGUMENTS. BVALU0665
66      C BVALUE=0.
67      C IF (JDERIV.GE.K) GO TO 170
68      C *** FIND I S.T. 1 .LE. I .LT. N+K AND T(I) .LT. T(I+1) AND
69      C T(I) .LE. X .LT. T(I+1) . IF NO SUCH I CAN BE FOUND, X LIES
70      C OUTSIDE THE SUPPORT OF THE SPLINE F AND BVALUE = 0.
71      C (THE ASYMMETRY IN THIS CHOICE OF I MAKES F RIGHTCONTINUOUS)
72      C CALL INTERV (T, N+K, X, I, MFLAG) BVALU073
73      C IF (MFLAG.NE.0) GO TO 170 BVALU074
74      C *** IF K = 1 (AND JDERIV = 0), BVALUE = BCOEF(I).
75      C KM1=K-1 BVALU075
76      C IF (KM1.GT.0) GO TO 16 BVALU076
77      C BVALUE=BCOEF(I) BVALU077
78      C GO TO 170 BVALU078
79      C
80      C *** STORE THE K B-SPLINE COEFFICIENTS RELEVANT FOR THE KNOT INTERVAL
81      C (T(I), T(I+1)) IN AJ(1), . . . , AJ(K) AND COMPUTE DL(J) = X - T(I+1-J), BVALU081
82      C DR(J) = T(I+J) - X, J=1, . . . , K-1 . SET ANY OF THE AJ NOT OBTAINABLE BVALU082
83      C FROM INPUT TO ZERO. SET ANY T.S NOT OBTAINABLE EQUAL TO T(1) OR BVALU083
84      C TO T(N+K) APPROPRIATELY. BVALU084
85      C JCMIN=1 BVALU085
86      C IMK= I-K BVALU086
87      C IF (IMK.GE.0) GO TO 40 BVALU087
88      C JCMIN=1-IMK BVALU088
89      C DO 20 J=1, I BVALU089
90      C L= I+1-J BVALU090
91      C DL(J)=X-T(L) BVALU091
92      C DO 30 J=1, KM1 BVALU092
93      C L=K-J BVALU093
94      C AJ(L)=0. BVALU094
95      C DL(J)=DL(I) BVALU095
96      C GO TO 60 BVALU096
97      C DO 50 J=1, KM1 BVALU097
98      C L= I+1-J BVALU098
99      C DL(J)=X-T(L) BVALU099
100      C
101      C JCMAX=K
102      C NM1=N-1 BVALU100
103      C IF (NM1.GE.0) GO TO 90 BVALU103
104      C JCMAX=K+NM1 BVALU104
105      C DO 70 J=1, JCMAX BVALU105
106      C L= I+J BVALU106
107      C DR(J)=T(L)-X BVALU107
108      C DO 80 J=JCMAX, KM1 BVALU108
109      C AJ(J+1)=0. BVALU109
110      C DR(J)=DR(JCMAX) BVALU110
111      C GO TO 110 BVALU111
112      C DO 100 J=1, KM1 BVALU112
113      C L= I+J BVALU113
114      C DR(J)=T(L)-X BVALU114
115      C

```

```

116      DO 120 JC=JCMIN,JCMAX
117      L=1MK+JC
118      AJ(JC)=BCOEF(L)
119
120      C      *** DIFFERENCE THE COEFFICIENTS  JDERIV  TIMES.
121      IF (JDERIV.EQ.0) GO TO 140
122      DO 130 J=1,JDERIV
123      KMJ=K-J
124      FKMJ=FLOAT(KMJ)
125      ILO=KMJ
126      DO 130 JJ=1,KMJ
127      AJ(JJ)=((AJ(JJ+1)-AJ(JJ))/(DL(ILO)+DR(ILO)))*FKMJ
128
129      ILO=ILO-1
130      C      *** COMPUTE VALUE AT  X  IN (T(I),T(I+1))  OF  JDERIV-TH DERIVATIVE,
131      C      GIVEN ITS RELEVANT B-SPLINE COEFFS IN AJ(1),...,AJ(K-JDERIV).
132      IF (JDERIV.EQ.KM1) GO TO 160
133      JDRV1=JDERIV+1
134      DO 150 J=JDRV1,KM1
135      KMJ=K-J
136      ILO=KMJ
137      DO 150 JJ=1,KMJ
138      AJ(JJ)=(AJ(JJ+1)*DL(ILO)+AJ(JJ)*DR(ILO))/(DL(ILO)+DR(JJ))
139      ILO=ILO-1
140      BVALUE=AJ(1)
141
142      C      RETURN
143      END
144

```

CPR*NS(1) . CHECK1(2)

```

1      SUBROUTINE CHECK1 (W,N,NX,KX,NKX,NY,NYX,JX,MO,AL,DL,C,NZ)      CHECK101
2
3      C----- CHECK1      WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING      CHECK102
4      C----- DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.      CHECK103
5      C----- AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION      CHECK104
6      C----- FOR: CHECKING WHETHER INPUT VALUES FALL WITHIN THEIR ALLOWABLE      CHECK105
7      C----- LIMITS      CHECK106
8      C----- SUBPROGRAMS CALLED: -NONE-      CHECK107
9      C----- CURRENT VERSION COMPLETED JUNE 20, 1980      CHECK108
10
11      DIMENSION W(NX)      CHECK109
12      C--- WRITE FORMATS      CHECK110
13      FORMAT ('/1X,21H*** VECTOR LENGTH N = ,14,2X,20H*EXCEEDS DIMENSIONED      CHECK111
14      2,10HVALUE NX = ,14)      CHECK112
15      FORMAT ('/1X,18H*** DIMENSION KX = ,14,2X,20H*MUST BE AT LEAST AS ,      CHECK113
16      2 8H>LARGE AS/5X,26H) + 2*(DEGREE OF SPLINE) = ,14)      CHECK114
17      FORMAT ('/1X,22H*** VECTOR LENGTH NY = ,14,2X,      CHECK115
18      2 20H*EXCEEDS DIMENSIONED ,11HVALUE NYX = ,14)      CHECK116
19      FORMAT ('/1X,17H*** WEIGHT NUMBER,15,1X,13H)IS NEGATIVE (,C10.5,1H)')      CHECK117
20      FORMAT ('/1X,22H*** DEGREE OF SPLINE (,13,12H) EXCEEDS 19)      CHECK118
21      FORMAT ('/1X,28H*** NUMBER OF OBSERVATIONS (,14,13H) MUST EXCEED,      CHECK119
22      2 15)      CHECK120
23      FORMAT ('/1X,33H*** ALPHA LEVEL OF SIGNIFICANCE (,F6.3,      CHECK121
24      2 10H) MUST BE ,21H)IN THE INTERVAL (0,1)      CHECK122
25      FORMAT ('/1X,33H*** DELTA LEVEL OF SIGNIFICANCE (,F6.3,      CHECK123
26      2 10H) MUST BE ,21H)IN THE INTERVAL (0,1)      CHECK124
27      FORMAT ('/1X,16H*** CONSTANT C (,F6.3,26H) MUST BE IN THE INTERVAL      CHECK125
28      2,11H)0.85,1,251)      CHECK126
29      FORMAT ('//1X,14,1X,40H*ERROR CONDITIONS DETECTED BY SUBROUTINE      CHECK127
30      2 8H*CHECK1*/6X,38H***PROGRAM EXECUTION TERMINATED***//')      CHECK128
31      FORMAT ('/1X,47H*** MAXIMUM ORDER OF SPLINES JX MUST BE 20 (NOT, 13,      CHECK129
32      2 1H)      CHECK130
33      FORMAT ('/5X,42HSEE APPENDIX 1 OF THE FOLLOWING NBS PAPER://5X,      CHECK131
34      2 36HA NEW APPROACH TO VOLUME CALIBRATION/5X,      CHECK132
35      3 51HBY J. A. LECHNER, C. P. REEVE, AND C. H. SPIEGELMAN/)      CHECK133
36      FORMAT ('/1X,23H*** VECTOR LENGTH N+K = ,14,2X,      CHECK134
37      2 20H*EXCEEDS DIMENSIONED ,11HVALUE NKX = ,14)      CHECK135
38      C--- INITIALIZE COUNT FOR ERROR CONDITIONS      CHECK136
39      COUNT=0      CHECK137
40      C--- INITIALIZE NUMBER OF ZERO WEIGHTS      CHECK138
41      NZ=0      CHECK139
42      C--- CHECK FOR VECTOR LENGTHS EXCEEDING DIMENSIONED VALUES      CHECK140
43      IF (N.LE.NX) GO TO 140      CHECK141
44      COUNT=COUNT+1      CHECK142
45      COUNT=COUNT+1      CHECK143
46      NK=N+K      CHECK144
47      IF (NK.LE.NKX) GO TO 150      CHECK145
48      COUNT=COUNT+1      CHECK146
49      WRITE (6,130) NK,NKX      CHECK147
50      K2=K+2*(MO-1)      CHECK148
51      IF (K2.LE.KX) GO TO 160      CHECK149
52      COUNT=COUNT+1      CHECK150
53      WRITE (6,20) KX,K2      CHECK151
54      IF (NY.LE.NYX) GO TO 170      CHECK152
55      COUNT=COUNT+1      CHECK153
56      WRITE (6,30) NY,NYX      CHECK154
57      C--- CHECK FOR NEGATIVE AND ZERO WEIGHTS      CHECK155

```

```

58      DO 200 I=1,N
59      IF (W(I)) 180,190,200
60      C--- COUNT EACH NEGATIVE WEIGHT AS AN ERROR CONDITION
61      KOUNT=KOUNT+1
62      WRITE (6,40) I,W(I)
63      GO TO 200
64      C--- COUNT ZERO WEIGHTS
65      NZ=NZ+1
66      CONTINUE
67      C--- CHECK FOR MAXIMUM ORDER OF SPLINE = 20
68      IF (JX.EQ.20) GO TO 210
69      KOUNT=KOUNT+1
70      WRITE (6,110) JX
71      C--- CHECK ORDER OF SPLINE
72      IF (MO.LE.20) GO TO 220
73      KOUNT=KOUNT+1
74      MD=MO-1
75      WRITE (6,50) MD
76      C--- CHECK NUMBER OF OBSERVATIONS
77      K2=K+MO-2+NZ
78      IF (N.GT.K2) GO TO 230
79      KOUNT=KOUNT+1
80      WRITE (6,60) N,K2
81      C--- CHECK SIGNIFICANCE LEVELS
82      IF (AL.GT.0.0.AND.AL.LE.1.0) GO TO 240
83      KOUNT=KOUNT+1
84      WRITE (6,70) AL
85      IF (DL.GT.0.0.AND.DL.LE.1.0) GO TO 250
86      KOUNT=KOUNT+1
87      WRITE (6,80) DL
88      C--- CHECK CONSTANT C
89      IF (C.LE.1.25.AND.C.GE.0.85) GO TO 260
90      KOUNT=KOUNT+1
91      WRITE (6,90) C
92      WRITE (6,120)
93      C--- CHECK WHETHER ANY ERROR CONDITIONS EXIST
94      IF (KOUNT.EQ.0) RETURN
95      WRITE (6,100) KOUNT
96      STOP
97      END

```

CPR*NSC(1) .CHECK2(1) SUBROUTINE CHECK2 (T, K, X, V, N, NX, NZ, MO)

C CHECK2 WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
 C DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D. C.
 C AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
 C FOR: CHECKING FOR OBSERVATIONS WHICH LIE OUTSIDE THE SEQUENCE OF
 C KNOTS. THE WEIGHTS OF SUCH OBSERVATIONS ARE SET TO ZERO.
 C SUBPROGRAMS CALLED: -NONE-
 C CURRENT VERSION COMPLETED MARCH 24, 1980

```

10
11      DIMENSION T(KX),X(NX),W(NX)
12      FORMAT ('/1X,6H*** X, 14,3H) =',G12.6,1X,22HIS OUTSIDE KNOT SPAN. .
13      2 1X,1HSET WEIGHT('14,5H) =0.')
14      20 FORMAT ('/1X,48H*** ADDITIONAL ZERO WEIGHTS GIVE NONPOSITIVE ***/9XCHECK214
15      2,32HDEGREES OF FREEDOM FOR RESIDUALS//6X,13H****PROGRAM ,
16      3 25HEXECUTION TERMINATED***//')
17      30 FORMAT ('/1X,15H*** VALUE OF X, 14,14H) CHANGED FROM, G14.8,2X,2HT0, CHECK217
18      2 G14.8/5X,45HS0 THAT IT WILL BE LESS THAN THE LARGEST KNOT)
19      DO 60 I=1,N
20      IF (W(I).EQ.0.0) GO TO 60
21      IF (X(I).LT.T(I)) GO TO 50
22      IF (X(I)-T(K) ) 60,40,50
23      XOLD=X(I)
24      X(I)=XOLD-ABS(XOLD)*0.00000001
25      WRITE (6,30) I,XOLD,X(I)
26      GO TO 60
27      50      W(I)=0.0
28      NZ=NZ+1
29      WRITE (6,10) I,X(I),I
30      CONTINUE
31      K2=K+MO-2+NZ
32      IF (N.GT.K2) RETURN
33      WRITE (6,20)
34      STOP
35      END
  
```

CPR*NS(1) . CHSCDF(1) SUBROUTINE CHSCDF (X, NU, CDF)

1 C
 2 C
 3 C
 4 C
 5 C
 6 C
 7 C
 8 C
 9 C
 10 C
 11 C
 12 C
 13 C
 14 C
 15 C
 16 C
 17 C
 18 C
 19 C
 20 C
 21 C
 22 C
 23 C
 24 C
 25 C
 26 C
 27 C
 28 C
 29 C
 30 C
 31 C
 32 C
 33 C
 34 C
 35 C
 36 C
 37 C
 38 C
 39 C
 40 C
 41 C
 42 C
 43 C
 44 C
 45 C
 46 C
 47 C
 48 C
 49 C
 50 C
 51 C
 52 C
 53 C
 54 C
 55 C
 56 C
 57 C

C PURPOSE--THIS SUBROUTINE COMPUTES THE CUMULATIVE DISTRIBUTION
 C FUNCTION VALUE FOR THE CHI-SQUARED DISTRIBUTION
 C WITH INTEGER DEGREES OF FREEDOM PARAMETER = NU.
 C THIS DISTRIBUTION IS DEFINED FOR ALL NON-NEGATIVE X.
 C THE PROBABILITY DENSITY FUNCTION IS GIVEN
 C IN THE REFERENCES BELOW.
 C INPUT ARGUMENTS--X = THE SINGLE PRECISION VALUE AT
 C WHICH THE CUMULATIVE DISTRIBUTION
 C FUNCTION IS TO BE EVALUATED.
 C X SHOULD BE NON-NEGATIVE.
 C --NU = THE INTEGER NUMBER OF DEGREES
 C OF FREEDOM.
 C NU SHOULD BE POSITIVE.
 C OUTPUT ARGUMENTS--CDF = THE SINGLE PRECISION CUMULATIVE
 C DISTRIBUTION FUNCTION VALUE.
 C OUTPUT--THE SINGLE PRECISION CUMULATIVE DISTRIBUTION
 C FUNCTION VALUE CDF FOR THE CHI-SQUARED DISTRIBUTION
 C WITH DEGREES OF FREEDOM PARAMETER = NU.
 C PRINTING--NONE UNLESS AN INPUT ARGUMENT ERROR CONDITION EXISTS.
 C RESTRICTIONS--X SHOULD BE NON-NEGATIVE.
 C --NU SHOULD BE A POSITIVE INTEGER VARIABLE.
 C OTHER DATAPAC SUBROUTINES NEEDED--NORCDF.
 C FORTRAN LIBRARY SUBROUTINES NEEDED--DSQRT, DEXP.
 C MODE OF INTERNAL OPERATIONS--DOUBLE PRECISION.
 C LANGUAGE--ANSI FORTRAN.
 C REFERENCES--NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS
 C SERIES 55, 1964, PAGE 941, FORMULAE 26.4.4 AND 26.4.5. CHSCD029
 C --JOHNSON AND KOTZ, CONTINUOUS UNIVARIATE
 C DISTRIBUTIONS--1, 1970, PAGE 176,
 C FORMULA 28, AND PAGE 180, FORMULA 33.1.
 C --OWEN, HANDBOOK OF STATISTICAL TABLES,
 C 1962, PAGES 50-55.
 C --PEARSON AND HARTLEY, BIOMETRICA TABLES
 C FOR STATISTICIANS, VOLUME 1, 1954,
 C PAGES 122-131.
 C WRITTEN BY--JAMES J. FILIBEN
 C STATISTICAL ENGINEERING LABORATORY (205.03)
 C NATIONAL BUREAU OF STANDARDS
 C WASHINGTON, D. C. 20234
 C PHONE: 301-921-2315
 C ORIGINAL VERSION--JUNE 1972.
 C UPDATED --MAY 1974.
 C UPDATED --SEPTEMBER 1975.
 C UPDATED --NOVEMBER 1975.
 C UPDATED --OCTOBER 1976.
 C
 C DOUBLE PRECISION DX, PI, CHI, SUM, TERM, AI, DCDFN
 C DOUBLE PRECISION DNU
 C DOUBLE PRECISION DSQRT, DEXP
 C DOUBLE PRECISION DLOG
 C DOUBLE PRECISION DFACT, DPOWER
 C DOUBLE PRECISION DW
 C DOUBLE PRECISION D1, D2, D3

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58      DOUBLE PRECISION TERM0, TERM1, TERM2, TERM3, TERM4
59      CHSCD058
59      CHSCD059
60      DOUBLE PRECISION B11
60      CHSCD060
61      DOUBLE PRECISION B21
61      CHSCD061
62      DOUBLE PRECISION B31, B32
62      CHSCD062
63      DOUBLE PRECISION B41, B42, B43
63      CHSCD063
64      DATA NUCUT /1000/
64      CHSCD064
64      DATA P1 /3. 14159265358979D0/
64      CHSCD065
65      DATA DPOWER /0. 333333333333333D0/
65      CHSCD066
66      DATA B11 /0. 33333333333333D0/
66      CHSCD067
67      DATA B21 /-0. 0277777777778D0/
67      CHSCD068
68      DATA B31 /-0. 00061728395061D0/
68      CHSCD069
69      DATA B32 /-13. 0D0/
69      CHSCD070
70      DATA B41 /0. 00018004115226D0/
70      CHSCD071
71      DATA B42 /6. 0D0/
71      CHSCD072
72      DATA B43 /17. 0D0/
72      CHSCD073
73      C
74      IPR=6
75      C      CHECK THE INPUT ARGUMENTS FOR ERRORS
76      C
77      C
78      IF (NU.LE.0) GO TO 10
78      IF (X.LT.0.0) GO TO 20
79      GO TO 30
80      10      WRITE (IPR, 50)
81      WRITE (IPR, 70) NU
82      CDF=0.0
83      RETURN
84      WRITE (IPR, 40)
85      WRITE (IPR, 60) X
86      CDF=0.0
87      RETURN
88      CONTINUE
89      30      FORMAT (1H, '96H***** NON-FATAL DIAGNOSTIC--THE FIRST INPUT ARGUMENT IS NEGATIVE *****')
90      40      2NT TO THE CHSCDF SUBROUTINE IS NEGATIVE ****)
91      50      FORMAT (1H, '91H***** FATAL ERROR--THE SECOND INPUT ARGUMENT TO THECHSCD092
92      2 CHSCDF SUBROUTINE IS NON-POSITIVE ****)
93      60      FORMAT (1H, '35H***** THE VALUE OF THE ARGUMENT IS ,E15.8, 6H *****) CHSCD094
94      60      FORMAT (1H, '35H***** THE VALUE OF THE ARGUMENT IS ,18,6H *****) CHSCD095
95      70      C
96      96      C      START POINT--_
97      97      C
98      DX=X
99      ANU=NU
100     DNU=NU
101     101     C
102     102     C
103     103     C
104     104     C
105     105     C
106     106     C
107     107     C
108     108     C
109     109     C
110     110     C
111     111     C
112     112     C
113     113     C
114     114     C
115     115     C
116     116     C
117     117     C
118     118     C
119     119     C
120     120     C
121     121     C
122     122     C
123     123     C
124     124     C
125     125     C
126     126     C
127     127     C
128     128     C
129     129     C
130     130     C
131     131     C
132     132     C
133     133     C
134     134     C
135     135     C
136     136     C
137     137     C
138     138     C
139     139     C
140     140     C
141     141     C
142     142     C
143     143     C
144     144     C
145     145     C
146     146     C
147     147     C
148     148     C
149     149     C
150     150     C
151     151     C
152     152     C
153     153     C
154     154     C
155     155     C
156     156     C
157     157     C
158     158     C
159     159     C
160     160     C
161     161     C
162     162     C
163     163     C
164     164     C
165     165     C
166     166     C
167     167     C
168     168     C
169     169     C
170     170     C
171     171     C
172     172     C
173     173     C
174     174     C
175     175     C
176     176     C
177     177     C
178     178     C
179     179     C
180     180     C
181     181     C
182     182     C
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116 C
117 IF (X.LE.0.0) GO TO 80
118 AMEAN=ANU
119 SD=SQRT(2.0*ANU)
120 Z=(X-AMEAN)/SD
121 IF (NU.LT.10.AND.Z.LT.-200.0) GO TO 80
122 IF (NU.GE.10.AND.Z.LT.-100.0) GO TO 80
123 IF (NU.LT.10.AND.Z.GT.200.0) GO TO 90
124 IF (NU.GE.10.AND.Z.GT.100.0) GO TO 90
125 GO TO 100
126 CDF=0.0
127 RETURN
128 CDF=1.0
129 RETURN
130 CONTINUE
131 C DISTINGUISH BETWEEN 3 SEPARATE REGIONS
132 C OF THE (X,NU) SPACE.
133 C BRANCH TO THE PROPER COMPUTATIONAL METHOD
134 C DEPENDING ON THE REGION.
135 C
136 C NUCUT HAS THE VALUE 1000.
137 C
138 IF (NU.LT.NUCUT) GO TO 120
139 IF (NU.GE.NUCUT.AND.X.LE.ANU) GO TO 180
140 IF (NU.GE.NUCUT.AND.X.GT.ANU) GO TO 190
141 IBRAN=1
142 WRITE (IPR,110) IBRAN
143 FORMAT (1H,'42H**** INTERNAL ERROR IN CHSCDF SUBROUTINE--',
144 2 '46HIMPOSSIBLE BRANCH CONDITION AT BRANCH POINT = ,18)
145 RETURN
146 C TREAT THE SMALL AND MODERATE DEGREES OF FREEDOM CASE
147 C (THAT IS, WHEN NU IS SMALLER THAN 1000).
148 C METHOD UTILIZED--EXACT FINITE SUM
149 C (SEE AMS 55, PAGE 941, FORMULAE 26.4.4 AND 26.4.5).
150 C
151 C
152 CONTINUE
153 CHI=DSQRT(DX)
154 IEVODD=NU-2*(NU/2)
155 IF (IEVODD.EQ.0) GO TO 130
156 C
157 SUM=0.0D0
158 TERM=1.0/CHI
159 IMIN=1
160 IMAX=NU-1
161 GO TO 140
162 SUM=1.0D0
163 TERM=1.0D0
164 IMIN=2
165 IMAX=NU-2
166 C
167 C
168 IF (IMIN.GT.IMAX) GO TO 160
169 DO 150 I=IMIN,IMAX,2
170 AI=1
171 TERM=TERM*(DX/AI)
172 SUM=SUM+TERM
173 CONTINUE

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174      CONTINUE
175      C
176      SUM=SUM*DEXP(-DX/2.0D0)
177      IF (IEVODD.EQ.0) GO TO 170
178      SUM=(DSQRT(2.0D0/PI))*SUM
179      SPCHI=CHI
180      CALL NORCDF (SPCHI, CDFN)
181      DCDFN=CDFN
182      SUM=SUM+2.0D0*(1.0D0-DCDFN)
183      CDF=1.0D0-SUM
184      RETURN
185      C
186      C TREAT THE CASE WHEN NU IS LARGE
187      C (THAT IS, WHEN NU IS EQUAL TO OR GREATER THAN 1000)
188      C AND X IS LESS THAN OR EQUAL TO NU.
189      C METHOD UTILIZED--WILSON-HILFERTY APPROXIMATION
190      C (SEE JOHNSON AND KOTZ, VOLUME 1, PAGE 176, FORMULA 28).
191      C
192      CONTINUE
193      DFACT=4.5D0*DNNU
194      U=((-DX/DNNU)**DPOWER)-1.0D0+(1.0D0/DFACT)*DSQRT(DFACT)
195      CALL NORCDF (U, CDFN)
196      CDF=CDFN
197      RETURN
198      C
199      C TREAT THE CASE WHEN NU IS LARGE
200      C (THAT IS, WHEN NU IS EQUAL TO OR GREATER THAN 1000)
201      C AND X IS LARGER THAN NU.
202      C METHOD UTILIZED--HILL'S ASYMPTOTIC EXPANSION
203      C (SEE JOHNSON AND KOTZ, VOLUME 1, PAGE 180, FORMULA 33.1).
204      C
205      CONTINUE
206      DW=DSQRT(DX-DNU-DNU*DLOG(DX/DNU))
207      DANU=DSQRT(2.0D0/DNU)
208      D1=DW
209      D2=DW**2
210      D3=DW**3
211      TERM0=DW
212      TERM1=B11*DANU
213      TERM2=B21*D1*(DANU**2)
214      TERM3=B31*(D2+B32)*(DANU**3)
215      TERM4=B41*(B42*D3+B43*D1)*(DANU**4)
216      U=TERM0+TERM1+TERM2+TERM3+TERM4
217      CALL NORCDF (U, CDFN)
218      CDF=CDFN
219      RETURN
220      C
221      END

```

CPR*NS(1).CHSPPF(1) SUBROUTINE CHSPPF (P,NU,PPF)

1 C
 2 C PURPOSE--THIS SUBROUTINE COMPUTES THE PERCENT POINT
 3 C FUNCTION VALUE FOR THE CHI-SQUARED DISTRIBUTION
 4 C WITH INTEGER DEGREES OF FREEDOM PARAMETER = NU.
 5 C THE CHI-SQUARED DISTRIBUTION USED
 6 C HEREIN IS DEFINED FOR ALL NON-NEGATIVE X,
 7 C AND ITS PROBABILITY DENSITY FUNCTION IS GIVEN
 8 C IN REFERENCES 2, 3, AND 4 BELOW.
 9 C
 10 C NOTE THAT THE PERCENT POINT FUNCTION OF A DISTRIBUTION
 11 C IS IDENTICALLY THE SAME AS THE INVERSE CUMULATIVE
 12 C DISTRIBUTION FUNCTION OF THE DISTRIBUTION.
 13 C INPUT ARGUMENTS--P = THE SINGLE PRECISION VALUE
 14 C (BETWEEN 0.0 (INCLUSIVELY)
 15 C AND 1.0 (EXCLUSIVELY))
 16 C AT WHICH THE PERCENT POINT
 17 C FUNCTION IS TO BE EVALUATED.
 18 C --NU = THE INTEGER NUMBER OF DEGREES
 19 C OF FREEDOM.
 20 C
 21 C OUTPUT ARGUMENTS--PPF = THE SINGLE PRECISION PERCENT
 22 C POINT FUNCTION VALUE.
 23 C
 24 C OUTPUT--THE SINGLE PRECISION PERCENT POINT FUNCTION
 25 C VALUE PPF FOR THE CHI-SQUARED DISTRIBUTION
 26 C WITH DEGREES OF FREEDOM PARAMETER = NU.
 27 C PRINTING--NONE UNLESS AN INPUT ARGUMENT ERROR CONDITION EXISTS.
 28 C RESTRICTIONS--NU SHOULD BE A POSITIVE INTEGER VARIABLE.
 29 C --P SHOULD BE BETWEEN 0.0 (INCLUSIVELY)
 30 C AND 1.0 (EXCLUSIVELY).
 31 C
 32 C OTHER DATAPAC SUBROUTINES NEEDED--NONE.
 33 C
 34 C LANGUAGE--ANSI FORTRAN.
 35 C ACCURACY--(ON THE UNIVAC 1108, EXEC 8 SYSTEM AT NBS)
 36 C COMPARED TO THE KNOWN NU = 2 (EXPONENTIAL)
 37 C RESULTS, AGREEMENT WAS HAD OUT TO 6 SIGNIFICANT
 38 C DIGITS FOR ALL TESTED P IN THE RANGE P = .001 TO
 39 C P = .999. FOR P = .95 AND SMALLER, THE AGREEMENT
 40 C WAS EVEN BETTER--7 SIGNIFICANT DIGITS.
 41 C (NOTE THAT THE TABULATED VALUES GIVEN IN THE WILK,
 42 C GNAADESIKAN, AND HUYETT REFERENCE BELOW, PAGE 20,
 43 C ARE IN ERROR FOR AT LEAST THE GAMMA = 1 CASE--
 44 C THE WORST DETECTED ERROR WAS AGREEMENT TO ONLY 3
 45 C SIGNIFICANT DIGITS (IN THEIR 8 SIGNIFICANT DIGIT TABLE)
 46 C FOR P = .999.)
 47 C REFERENCES--WILK, GNAADESIKAN, AND HUYETT, 'PROBABILITY
 48 C PLOTS FOR THE GAMMA DISTRIBUTION',
 49 C TECHNOMETRICS, 1962, PAGES 1-15,
 50 C ESPECIALLY PAGES 3-5.
 51 C
 52 C --NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS
 53 C SERIES 55, 1964, PAGE 257, FORMULA 6.1.41,
 54 C AND PAGES 940-943.
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 56 C --JOHNSON AND KOTZ, CONTINUOUS UNIVARIATE
 57 C DISTRIBUTIONS--1, 1970, PAGES 166-206.
 58 C
 59 C --HASTINGS AND PEACOCK, STATISTICAL
 60 C DISTRIBUTIONS--A HANDBOOK FOR
 61 C STUDENTS AND PRACTITIONERS, 1975.

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PAGES 46-51.  
C 59 C DOUBLE PRECISION DP, DCAMMA  
C 60 C DOUBLE PRECISION Z, Z2, Z3, Z4, Z5, DEN, A, B, C, D, G  
C 61 C DOUBLE PRECISION XMIN0, XMIN, AI, XMAX, DX, PCALC, XMID  
C 62 C DOUBLE PRECISION XLOWER, XUPPER, XDEL  
C 63 C DOUBLE PRECISION SUM, TERM, CUT1, CUT2, AJ, CUTOFF, T  
C 64 C DOUBLE PRECISION DEXP, DLLOG  
C 65 C DIMENSION D(10)  
C 66 C DATA C / .9 18938533204672741D0 /  
C 67 C DATA D(1), D(2), D(3), D(4), D(5) / + .833333333333333D-1,  
C 68 C 2 / -.2277777777777778D-2, + .793650793650793651D-3,  
C 69 C 3 / .595238095238095238D-3, + .841750841750841751D-3 /  
C 70 C DATA D(6), D(7), D(8), D(9), D(10) / - .191752691752691753D-2,  
C 71 C 2 / .641025641025641025D-2, - .29550653594712418D-1,  
C 72 C 3 / .179644372368839573D0, - .139243221690590111D1 /  
C 73 C  
C 74 C IPR=6  
C 75 C  
C 76 C CHECK THE INPUT ARGUMENTS FOR ERRORS  
C 77 C IF (P.LT.0.0.OR.P.GE.1.0) GO TO 10  
C 78 C IF (NU.LT.1) GO TO 20  
C 79 C GO TO 30  
C 80 C  
C 81 C 10 WRITE (IPR,40)  
C 82 C 92 WRITE (IPR,60) P  
C 83 C 93 PPF=0.0  
C 84 C 94 RETURN  
C 85 C 95 WRITE (IPR,50)  
C 86 C 96 WRITE (IPR,70) NU  
C 87 C 97 PPF=0.0  
C 88 C 98 RETURN  
C 89 C 99 CONTINUE  
C 90 C 100 FORMAT (1H ,11H****) FATAL ERROR--THE FIRST INPUT ARGUMENT TO THCHISPP100  
C 91 C 101 2E CHISPP SUBROUTINE IS OUTSIDE THE ALLOWABLE (0, 1) INTERVAL *****) CHISPP101  
C 92 C 102 FORMAT (1H ,91H****) FATAL ERROR--THE SECOND INPUT ARGUMENT TO THECHISPP102  
C 93 C 103 2 CHISPP SUBROUTINE IS NON-POSITIVE *****) CHISPP103  
C 94 C 104 FORMAT (1H ,35H****) THE VALUE OF THE ARGUMENT IS ,E15.8, 6H *****) CHISPP104  
C 95 C 105 FORMAT (1H ,35H****) THE VALUE OF THE ARGUMENT IS ,18, 6H *****) CHISPP105  
C 96 C 106 C  
C 97 C-----START POINT-----  
C 107 C  
C 108 C EXPRESS THE CHI-SQUARED DISTRIBUTION PERCENT POINT  
C 109 C FUNCTION IN TERMS OF THE EQUIVALENT GAMMA  
C 110 C DISTRIBUTION PERCENT POINT FUNCTION,  
C 111 C AND THEN EVALUATE THE LATTER.  
C 112 C  
C 113 C ANU=NU  
C 114 C GAMMA=ANU/2.0  
C 115 C
```

```

116      DF=P
117      DNU=NU
118      DGAMMA=DNU/2.0D0
119      MAXIT=10000
120      C COMPUTE THE GAMMA FUNCTION USING THE ALGORITHM IN THE
121      C NBS APPLIED MATHEMATICS SERIES REFERENCE.
122      C THIS GAMMA FUNCTION NEED BE CALCULATED ONLY ONCE.
123      C IT IS USED IN THE CALCULATION OF THE GPF BASED ON
124      C THE TENTATIVE VALUE OF THE PPF IN THE ITERATION.
125      C
126      C
127      Z=DGAMMA
128      DEN=1.0D0
129      80      IF (Z.GE.10.0D0) GO TO 90
130      DEN=DEN*Z
131      Z=Z+1.0D0
132      GO TO 80
133      90      72=Z*Z
134      Z3=Z*Z2
135      Z4=Z2*Z2
136      Z5=Z2*Z3
137      A=(Z-0.5D0)*DLOG(Z)-Z+C
138      B=D(1)/Z+D(2)/Z3+D(3)/Z5+D(4)/(Z2*Z5)+D(5)/(Z4*Z5)+D(6)/(Z2*Z3*Z5)+D(7)/(Z3*Z5*Z5)+D(8)/(Z5*Z3*Z5)+D(9)/(Z2*Z3*Z5*Z5)
139      C=DEXP(A+B)/DEN
140
141      C DETERMINE LOWER AND UPPER LIMITS ON THE DESIRED PPF
142      C PERCENT POINT.
143      C
144      C
145      ILOOP=1
146      XMIN=(DF*DGAMMA*G)**(1.0D0/DGAMMA)
147      XMIN=XMIN
148      ICOUNT=1
149      AI=ICOUNT
150      XMAX=AI*XMIN
151      DX=XMAX
152      GO TO 160
153      IF (PCALC.GE.DP) GO TO 120
154      XMIN=XMAX
155      ICOUNT=ICOUNT+1
156      IF (ICOUNT.LE.30000) GO TO 100
157      XMID=(XMIN+XMAX)/2.0D0
158      C
159      C NOW ITERATE BY BISECTION UNTIL THE DESIRED ACCURACY IS ACHIEVED.
160      C
161      ILOOP=2
162      XLOWER=XMIN
163      XUPPER=XMAX
164      ICOUNT=0
165      DX=XMID
166      GO TO 160
167      IF (PCALC.EQ.DP) GO TO 170
168      IF (PCALC.GT.DP) GO TO 150
169      XLOWER=XMID
170      XMID=(XMID+XUPPER)/2.0D0
171      GO TO 160
172      XUPPER=XMID
173      XMID=(XMID+XLOWER)/2.0D0

```

```

174      XDEL=XMIN-XLOWER
175      IF ( XDEL.LT.0.0D0) XDEL=-XDEL
176      ICOUNT= ICOUNT+1
177      IF ( XDEL.LT.0.0D0) GO TO 130
178      GO TO 130
179      PPF=2.0D0*XMIN
180      RETURN
181      C*****
182      C THIS SECTION BELOW IS LOGICALLY SEPARATE FROM THE ABOVE.
183      C THIS SECTION COMPUTES A CDF VALUE FOR ANY GIVEN TENTATIVE
184      C PERCENT POINT X VALUE AS DEFINED IN EITHER OF THE 2
185      C ITERATION LOOPS IN THE ABOVE CODE.
186      C
187      C COMPUTE T-SUB-Q AS DEFINED ON PAGE 4 OF THE WILK, GNANADESIKAN,
188      C AND HUYETT REFERENCE
189      C
190      180      SUM=1.0D0/DGAMMA
191      TERM=1.0D0/DGAMMA
192      CUT1=DX-DGAMMA
193      CUT2=DX*10000000000.0D0
194      DO 190 J=1,MAXIT
195      196      AJ=J
196      TERM=DX*TERM/( DGAMMA+AJ)
197      SUM=SUM+TERM
198      CUTOFF=CUT1+(CUT2*TERM/SUM)
199      IF (AJ.GT.CUTOFF) GO TO 200
200      CONTINUE
201      190      WRITE ( IPR, 210) MAXIT
202      WRITE ( IPR, 220) P
203      WRITE ( IPR, 230) NU
204      WRITE ( IPR, 240)
205      PPF=0.0
206      RETURN
207
208      200      T=SUM
209      PCALC=(DX**DGAMMA)*(DEXP(-DX))*T/G
210      IF ( ILOOP.EQ. 1) GO TO 110
211      GO TO 140
212
213      C
214      210      FORMAT ( 1H ,48H*****ERROR IN INTERNAL OPERATIONS IN THE CHSPPF
215      2 45HSUBROUTINE--THE NUMBER OF ITERATIONS EXCEEDS 17),
216      220      FORMAT ( 1H ,33H      THE INPUT VALUE OF P IS ,E15.8)
217      230      FORMAT ( 1H ,33H      THE INPUT VALUE OF NU IS ,I8)
218      240      FORMAT ( 1H ,48H      THE OUTPUT VALUE OF PPF HAS BEEN SET TO 0.0)
219      C
220

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CPR*NS(1) .CIYFIN(6) SUBROUTINE CIYFIN (XF, YF, YFSD, NF, RSD, AL, DL, C, NRS, NB, YFL, YFU, IP) CIYFIN01
1
2 C--- CIYFIN WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING CIYFIN02
3 C DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C. CIYFIN03
4 C AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION CIYFIN04
5 C FOR: COMPUTING CONFIDENCE INTERVALS FOR PREDICTED Y-VALUES ON A CIYFIN05
6 C CALIBRATION CURVE USING SCHEFFE'S TECHNIQUE CIYFIN06
7 C CIYFIN07
8 C CIYFIN08
9 C REFERENCE: SCHEFFE, HENRY, 'A STATISTICAL THEORY OF CALIBRATION' CIYFIN09
10 C THE ANNALS OF STATISTICS, VOLUME 1, NUMBER 1 CIYFIN10
11 C JANUARY 1973, PP. 1-37 CIYFIN11
12 C
13 C SUBPROGRAMS CALLED: CHSPPF, FPPF, NORPPF CIYFIN12
14 C CURRENT VERSION COMPLETED MARCH 17, 1980 CIYFIN13
15 C CIYFIN14
16 C--- DIMENSION XF(NF), YF(NF), YFSD(NF), YFL(NF), YFU(NF) CIYFIN15
17 C--- WRITE FORMATS CIYFIN16
18 10 FORMAT (15X, 2HZ, 'F7.5, 3H) =, F11.5) CIYFIN17
19 20 FORMAT (6X, 6CHHSQ(, F7.5, 1H, 'I4, 3H) =, F11.5) CIYFIN18
20 30 FORMAT (5X, 2HFC(, F7.5, 1H, 'I4, 1H, 'I4, 3H) =, F11.5) CIYFIN19
21 40 FORMAT ('/1X, 75(1H-) /1X, 26H* CONFIDENCE INTERVALS FOR, I5, 1X, CIYFIN20
22 2 43HEVENLY SPACED POINTS WITHIN THE KNOT SPAN */1X, 75(1H-) //5X, CIYFIN21
23 3 7HALPHA =, F8.5, 5X, 7HDELTA =, F8.5, 5X, 3HC =, F5.2/) CIYFIN22
24 50 FORMAT ('1X, 14.5G13.6) CIYFIN23
25 60 FORMAT ('/20X, 9HPREDICTED, 5X, 7HSTD DEV, 6X, 19HCONFIDENCE INTERVAL, CIYFIN24
26 2 4X, 1H, 5X, 4HX1), 9X, 4HY1), 6X, 9HPRED Y1), 6X, 5HLOWER, 6X, 5HUPPER,) CIYFIN25
27 27 WRITE (6, 40) NF, AL, DL, C CIYFIN26
28 C--- COMPUTE Z(1-AL/2) CRITICAL POINT FOR N(0, 1) P.D.F. CIYFIN27
29 P=1.0-AL/2.0 CIYFIN28
30 CALL NORPPF (P, ZAL) CIYFIN29
31 WRITE (6, 10) P, ZAL CIYFIN30
32 C--- ARTIFICIALLY SET NEXT TWO CRITICAL POINTS IF DELTA=1 CIYFIN31
33 CDL=NRS, FDL=0 CIYFIN32
34 P=1.0-DL CIYFIN33
35 IF (DL.EQ.1.0) GO TO 70 CIYFIN34
36 C--- COMPUTE CHISQ(DL) CRITICAL POINT FOR CHI-SQUARED(NRS) P.D.F. CIYFIN35
37 CALL CHSPPF (DL, NRS, CDL) CIYFIN36
38 WRITE (6, 20) DL, NRS, CDL CIYFIN37
39 C--- COMPUTE F(1-DL) CRITICAL POINT FOR F(NB, NRS) P.D.F. CIYFIN38
40 CALL FPPF (P, NB, NRS, FDL) CIYFIN39
41 WRITE (6, 30) P, NB, NRS, FDL CIYFIN40
42 C--- COMPUTE CONFIDENCE INTERVAL FOR EACH Y VALUE CIYFIN41
43 C1=ZAL*SQRT(FLOAT(NRS)/CDL) CIYFIN42
44 C2=SQRT(FLOAT(NB)*FDL) CIYFIN43
45 C3=C*RSDF CIYFIN44
46 DO 80 I=1, NF CIYFIN45
47 WIDTH=C3*(C1+C2*YFSD(1)) CIYFIN46
48 YFL(1)=YF(1)-WIDTH CIYFIN47
49 YFU(1)=YF(1)+WIDTH CIYFIN48
50 CONTINUE CIYFIN49
51 C--- CHECK WHETHER TO PRINT OUT EACH Y VALUE AND ITS STANDARD DEVIATION CIYFIN50
52 IF (IP.LT.2) GO TO 100 CIYFIN51
53 C--- PRINT OUT EACH Y VALUE AND ITS STANDARD DEVIATION CIYFIN52
54 WRITE (6, 60) CIYFIN53
55 DO 90 I=1, NF CIYFIN54
56 WRITE (6, 50) I, XF(1), YF(1), YFSD(1), YFL(1), YFU(1) CIYFIN55
57 CIYFIN56
58 CIYFIN57

```

58 90 CONTINUE
59 RETURN
60 100 WRITE (6,110)
61 110 FORMAT ('/1X,43H***** PRINTOUT OF Y CONFIDENCE INTERVALS',
62 2 18HSUPPRESSED *****)
63 RETURN
64 END

CIYF IN58
CIYF IN59
CIYF IN60
CIYF IN61
CIYF IN62
CIYF IN63
CIYF IN64

```

CPR*NS(1) COVAR(2) SUBROUTINE COVAR (NNX,N,KMX,K,Q,CI)
1      C
2      C
3      C      INTEGER NMX,N,KMX,K
4      C      REAL Q(KMX,N),CI(NMX,N)
5      C
6      C      THIS FORTRAN SUBROUTINE COMPUTES AND RETURNS THE N X N UNSCALED
7      C      COVARIANCE MATRIX CI OBTAINED BY INVERTING THE GRAMIAN MATRIX C.  THE
8      C      CHOLESKY FACTOR L OF C IS ASSUMED TO BE STORED IN Q ON INPUT.
9      C      SUBROUTINE BCHSLV IS USED TO SOLVE FOR EACH COLUMN OF THE INVERSE.
10     C
11     C      ON INPUT.
12     C
13     C      NMX      IS THE ROW DIMENSION OF CI.
14     C
15     C      N       IS THE DIMENSION OF THE SPACE OF SPLINES OF ORDER
16     C                  K.
17     C
18     C      KMX      IS THE ROW DIMENSION OF Q.
19     C
20     C      K       IS THE ORDER OF THE SPLINES = DEGREE + 1
21     C
22     C      Q(*,*)   HAS ROW DIMENSION KMX AND COLUMN DIMENSION AT LEAST COVAR022
23     C
24     C      *       N.  THE CHOLESKY FACTOR L OF C IS STORED IN THE
25     C                  FIRST K ROWS OF THE MATRIX.
26     C
27     C      ON OUTPUT.
28     C      CI(*,*)   HAS ROW DIMENSION NMX AND COLUMN DIMENSION AT LEAST COVAR028
29     C
30     C      *       N.  IT CONTAINS THE UNSCALED COVARIANCE MATRIX IN
31     C                  STANDARD ROW, COLUMN FORM.
32     C
33     C      AND THE REST OF THE VARIABLES ARE UNCHANGED.
34     C
35     C      ADDITIONAL ROUTINES REQUIRED.
36     C      BCHSLV
37     C
38     C      BY.
39     C
40     C      MARTIN CORDEES
41     C      CENTER FOR APPLIED MATHEMATICS, NBS
42     C      VERSION 1 - OCT 1979
43     C
44     C
45     C      INTEGER I,J
46     C
47     C      DO 20 J=1,N
48     C      DO 10 I=1,N
49     C      CI(I,J)=0.0
50     C
51     C      10    CONTINUE
52     C      CI(J,J)=1.0
53     C      CALL BCHSLV (Q,KMX,K,N,CI(1,J))
54     C      CONTINUE
55     C
56     C      RETURN
57     C

```

1 C SUBROUTINE FCDF (X, NU1, NU2, CDF)
 2 C
 3 C PURPOSE-- THIS SUBROUTINE COMPUTES THE CUMULATIVE DISTRIBUTION
 4 C FUNCTION VALUE FOR THE F DISTRIBUTION
 5 C WITH INTEGER DEGREES OF FREEDOM
 6 C
 7 C PARAMETERS = NU1 AND NU2.
 8 C
 9 C INPUT ARGUMENTS--X = THIS DISTRIBUTION IS DEFINED FOR ALL NON-NEGATIVE X.
 10 C THE PROBABILITY DENSITY FUNCTION IS GIVEN
 11 C IN THE REFERENCES BELOW.
 12 C
 13 C
 14 C
 15 C
 16 C
 17 C
 18 C
 19 C
 20 C
 21 C
 22 C
 23 C
 24 C
 25 C
 26 C
 27 C
 28 C
 29 C
 30 C
 31 C
 32 C
 33 C
 34 C
 35 C
 36 C
 37 C
 38 C
 39 C
 40 C
 41 C
 42 C
 43 C
 44 C
 45 C
 46 C
 47 C
 48 C
 49 C
 50 C
 51 C
 52 C
 53 C
 54 C
 55 C
 56 C
 57 C

C COMPUTES THE CUMULATIVE DISTRIBUTION
 C WITH INTEGER DEGREES OF FREEDOM
 C
 C THIS DISTRIBUTION IS DEFINED FOR ALL NON-NEGATIVE X.
 C THE PROBABILITY DENSITY FUNCTION IS GIVEN
 C IN THE REFERENCES BELOW.
 C
 C ARGUMENTS--X = THE SINGLE PRECISION VALUE AT
 C WHICH THE CUMULATIVE DISTRIBUTION
 C FUNCTION IS TO BE EVALUATED.
 C X SHOULD BE NON-NEGATIVE.
 C
 C --NU1 = THE INTEGER DEGREES OF FREEDOM
 C FOR THE NUMERATOR OF THE F RATIO.
 C NU1 SHOULD BE POSITIVE.
 C
 C --NU2 = THE INTEGER DEGREES OF FREEDOM
 C FOR THE DENOMINATOR OF THE F RATIO.
 C NU2 SHOULD BE POSITIVE.
 C
 C OUTPUT ARGUMENTS--CDF = THE SINGLE PRECISION CUMULATIVE
 C DISTRIBUTION FUNCTION VALUE.
 C
 C OUTPUT--THE SINGLE PRECISION CUMULATIVE DISTRIBUTION
 C FUNCTION VALUE CDF FOR THE F DISTRIBUTION
 C WITH DEGREES OF FREEDOM
 C
 C PRINTING--NONE UNLESS AN INPUT ARGUMENT ERROR CONDITION EXISTS.
 C
 C RESTRICTIONS--X SHOULD BE NON-NEGATIVE.
 C --NU1 SHOULD BE A POSITIVE INTEGER VARIABLE.
 C --NU2 SHOULD BE A POSITIVE INTEGER VARIABLE.
 C
 C OTHER DATAPAC SUBROUTINES NEEDED--NORCDF, CHISCDF.
 C FORTRAN LIBRARY SUBROUTINES NEEDED--DSQRT, DATAN.
 C MODE OF INTERNAL OPERATIONS--DOUBLE PRECISION.
 C LANGUAGE--ANSI FORTRAN.
 C
 C REFERENCES--NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS
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 C
 C

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58      C
59      DOUBLE PRECISION DX,P1,ANU1,ANU2,Z,SUM,TERM,AI,COEFF1,COEFF2,ARG
60      DOUBLE PRECISION COEF
61      DOUBLE PRECISION THETA,SINTH,COSTH,A,B
62      DOUBLE PRECISION DSQRT, DATAN
63      DOUBLE PRECISION DFACT1,DFACT2,DNUM,DDEN
64      DOUBLE PRECISION DP0W1,DP0W2
65      DOUBLE PRECISION DNU1,DNU2
66      DOUBLE PRECISION TERM1,TERM2,TERM3
67      DATA PI /3.14159265358979D0/
68      DATA DP0W1,DP0W2 /0.333333333333D0,0.666666666666667D0/
69      DATA NUCUT1,NUCUT2 /100,1000/
70
71      C
72      C
73      C      CHECK THE INPUT ARGUMENTS FOR ERRORS
74      C
75      IF (NU1.LE.0) GO TO 10
76      IF (NU2.LE.0) GO TO 20
77      IF (X.LT.0.0) GO TO 30
78      GO TO 40
79      WRITE (IPR,60)
80      WRITE (IPR,90) NU1
81      CDF=0.0
82      RETURN
83      WRITE (IPR,70)
84      WRITE (IPR,90) NU2
85      CDF=0.0
86      RETURN
87      WRITE (IPR,50)
88      WRITE (IPR,80) X
89      CDF=0.0
90      RETURN
91      CONTINUE
92      FORMAT (1H,'96H**** NON-FATAL DIAGNOSTIC--THE FIRST INPUT ARGUMENT
93      2NT TO THE FCDF SUBROUTINE IS NEGATIVE ****')
94      60      FORMAT (1H,'91H**** FATAL ERROR--THE SECOND INPUT ARGUMENT TO THE
95      2 FCDF SUBROUTINE IS NON-POSITIVE ****')
96      70      FORMAT (1H,'91H**** FATAL ERROR--THE THIRD INPUT ARGUMENT TO THE
97      2 FCDF SUBROUTINE IS NON-POSITIVE ****')
98      80      FORMAT (1H,'35H**** THE VALUE OF THE ARGUMENT IS ,E15.8,6H ****)
99      90      FORMAT (1H,'35H**** THE VALUE OF THE ARGUMENT IS ,18,6H ****)
100     C
101     C      --START POINT--
```

```

102     C
103     DX=X
104     M=NU1
105     N=NU2
106     ANU1=NU1
107     ANU2=NU2
108     DNU1=NU1
109     DNU2=NU2
110
111     C      IF X IS NON-POSITIVE, SET CDF = 0.0 AND RETURN.
112     C      IF NU2 IS 5 THROUGH 9 AND X IS MORE THAN 3000
113     C      STANDARD DEVIATIONS BELOW THE MEAN,
114     C      SET CDF = 0.0 AND RETURN.
115     C      IF NU2 IS 10 OR LARGER AND X IS MORE THAN 150
```

```

116      C STANDARD DEVIATIONS BELOW THE MEAN,
117      C SET CDF = 0.0 AND RETURN.
118      C IF NU2 IS 5 THROUGH 9 AND X IS MORE THAN 3000
119      C STANDARD DEVIATIONS ABOVE THE MEAN,
120      C SET CDF = 1.0 AND RETURN.
121      C IF NU2 IS 10 OR LARGER AND X IS MORE THAN 150
122      C STANDARD DEVIATIONS ABOVE THE MEAN,
123      C SET CDF = 1.0 AND RETURN.
124      C
125      IF (X.LE.0.0) GO TO 100
126      IF (NU2.LE.4) GO TO 120
127      T1=2.0/ANU1
128      T2=ANU2/(ANU2-2.0)
129      T3=(ANU1+ANU2-2.0)/(ANU2-4.0)
130      ANEAN=T2
131      SD=SQRT(T1*T2*T2*T3)
132      ZRATIO=(X-ANEAN)/SD
133      IF (NU2.LT.10.AND.ZRATIO.LT.-3000.0) GO TO 100
134      IF (NU2.GE.10.AND.ZRATIO.LT.-150.0) GO TO 100
135      IF (NU2.LT.10.AND.ZRATIO.GT.3000.0) GO TO 110
136      IF (NU2.GE.10.AND.ZRATIO.GT.150.0) GO TO 110
137      GO TO 120
138      CDF=0.0
139      RETURN
140      CDF=1.0
141      RETURN
142      120  CONTINUE
143      C
144      C DISTINGUISH BETWEEN 6 SEPARATE REGIONS
145      C OF THE (NU1,NU2) SPACE.
146      C BRANCH TO THE PROPER COMPUTATIONAL METHOD
147      C DEPENDING ON THE REGION.
148      C NUCUT1 HAS THE VALUE 100.
149      C NUCUT2 HAS THE VALUE 1000.
150      C
151      IF (NU1.LT.NUCUT2.AND.NU2.LT.NUCUT2) GO TO 140
152      IF (NU1.GE.NUCUT2.AND.NU2.GE.NUCUT2) GO TO 310
153      IF (NU1.LT.NUCUT1.AND.NU2.GE.NUCUT2) GO TO 320
154      IF (NU1.GE.NUCUT1.AND.NU2.GE.NUCUT2) GO TO 310
155      IF (NU1.GE.NUCUT2.AND.NU2.LT.NUCUT1) GO TO 330
156      IF (NU1.GE.NUCUT2.AND.NU2.GE.NUCUT1) GO TO 310
157      IBRAN=5
158      WRITE (IPR,130) IBRAN
159      FORMAT (1H,'42H**** INTERNAL ERROR IN FCDF SUBROUTINE--,
160      2 46HIMPOSSIBLE BRANCH CONDITION AT BRANCH POINT = ,18)
161      RETURN
162      C
163      C TREAT THE CASE WHEN NU1 AND NU2
164      C ARE BOTH SMALL OR MODERATE
165      C (THAT IS, BOTH ARE SMALLER THAN 1000).
166      C METHOD UTILIZED--EXACT FINITE SUM
167      C (SEE AMS 55, PAGE 946, FORMULAE 26.6.4, 26.6.5,
168      C AND 26.6.8).
169      C
170      CONTINUE
171      Z=ANU2/(ANU2+ANU1*DX)
172      IFLAG1=NU1-2*(NU1/2)
173      IFLAG2=NU2-2*(NU2/2)

```

```

174      IF ( IFLAG1.EQ.0) GO TO 150
175      IF ( IFLAG2.EQ.0) GO TO 210
176      GO TO 210
177      C
178      C      DO THE NU1 EVEN AND NU2 EVEN OR ODD CASE
179      C
180      150      SUM=0. 0D0
181      TERM=1. 0D0
182      IMAX=(N-2)/2
183      IF ( IMAX.LE.0) GO TO 170
184      DO 160 I=1, IMAX
185      AI=I
186      COEF1=2. 0D0*( AI-1. 0D0)
187      COEF2=2. 0D0*AI
188      TERM=TERM*( ( ANU2+COEF1)/COEF2)*( 1. 0D0-Z)
189      SUM=SUM+TERM
190      SUM=( Z**2*( ANU2/2. 0D0))*SUM
191      CDF=1. 0D0-SUM
192      RETURN
193
194
195
196      C      DO THE NU1 ODD AND NU2 EVEN CASE
197      C
198      198      SUM=0. 0D0
199      TERM=1. 0D0
200      IMAX=(N-2)/2
201      IF ( IMAX.LE.0) GO TO 200
202      DO 190 I=1, IMAX
203      AI=I
204      COEF1=2. 0D0*( AI-1. 0D0)
205      COEF2=2. 0D0*AI
206      TERM=TERM*( ( ANU1+COEF1)/COEF2)*Z
207      SUM=SUM+TERM
208      RETURN
209
210      C      DO THE NU1 ODD AND NU2 ODD CASE
211      C
212      SUM=( ( 1. 0D0-Z)**(ANU1/2. 0D0))*SUM
213      RETURN
214
215      C      DO THE NU1 ODD AND NU2 ODD CASE
216      C
217      216      SUM=0. 0D0
218      TERM=1. 0D0
219      ARG=DSQRT( ( ANU1/ANU2)*DX)
220      THETA=DATAN( ARG)
221      SINH=ARG/DSQRT( 1. 0D0+ARG*ARG)
222      COSTH=1. 0D0/DSQRT( 1. 0D0+ARG*ARG)
223      IF ( N.EQ.1) GO TO 240
224      IF ( N.EQ.3) GO TO 230
225      IMAX=N-2
226      DO 220 I=3, IMAX, 2
227      AI=I
228      COEF1=AI-1. 0D0
229      COEF2=AI
230      TERM=TERM*( COEF1/COEF2)*(COSTH*COSTH)
231      SUM=SUM+TERM

```

```

229  CONTINUE
230  C      SUM=SUM+ 1.0D0
231  C      SUM=SUM*SINTH*COSTH
232  C
233  C
234  C
235  C
236  C      A=(2.0D0/P1)*(THETA+SUM)
237  C      SUM=0.0D0
238  C      TERM=1.0D0
239  C      IF (M.EQ. 1) B=0.0D0
240  C      IF (M.EQ. 1) GO TO 300
241  C      IF (M.EQ. 3) GO TO 260
242  C      IF (M.EQ. 3) GO TO 260
243  C      IMAX=M-3
244  DO 250 I= 1, IMAX, 2
245  AI= I
246  COEF1=AI
247  COEF2=AI+2.0D0
248  TERM=TERM*( (ANU2+COEF1) /COEF2)*(SINTH*SINTH)
249  SUM=SUM+TERM
250  CONTINUE
251  C
252  SUM=SUM+1.0D0
253  SUM=SUM*SINTH*(COSTH*N)
254  COEF=1.0D0
255  IEVODD=N-2*(N/2)
256  IMIN=3
257  IF (IEVODD.EQ. 0) IMIN=2
258  IF (IMIN.GT. N) GO TO 280
259  DO 270 I=IMIN,N,2
260  AI= I
261  COEF=((AI-1.0D0)/AI)*COEF
262  CONTINUE
263  C
264  COEF=COEF*ANU2
265  IF (IEVODD.EQ. 0) GO TO 290
266  COEF=COEF*(2.0D0/P1)
267  C
268  B=COEF*SUM
269  C
270  CDF=A-B
271  RETURN
272  C
273  C      TREAT THE CASE WHEN NU1 AND NU2
274  C      ARE BOTH LARGE
275  C      (THAT IS, BOTH ARE EQUAL TO OR LARGER THAN 1000);
276  C      OR WHEN NU1 IS MODERATE AND NU2 IS LARGE
277  C      (THAT IS, WHEN NU1 IS EQUAL TO OR GREATER THAN 100
278  C      BUT SMALLER THAN 1000,
279  C      AND NU2 IS EQUAL TO OR LARGER THAN 1000);
280  C      OR WHEN NU2 IS MODERATE AND NU1 IS LARGE
281  C      (THAT IS, WHEN NU2 IS EQUAL TO OR GREATER THAN 100
282  C      BUT SMALLER THAN 1000,
283  C      AND NU1 IS EQUAL TO OR LARGER THAN 1000).
284  C      METHOD UTILIZED-PAULSON APPROXIMATION
285  C      (SEE AMS 55, PAGE 947, FORMULA 26.6.15).
286  C
287  CONTINUE
288  DFACT1=1.0D0/(4.5D0*DN1)
289  DFACT2=1.0D0/(4.5D0*DN2)

```

```

DNUM=((1.0D0-DFACT2)*(DX**DPOW1))-(1.0D0-DFACT1)
DDEN=DSQRT((DFACT2*(DX**DPOW2))+DFACT1)
U=DNUM/DDEN
CALL NORCDF (U,GCDF)
CDF=GCDF
RETURN
C
296
297 C TREAT THE CASE WHEN NU1 IS SMALL
298 C AND NU2 IS LARGE
299 C ( THAT IS, WHEN NU1 IS SMALLER THAN 100,
300 C AND NU2 IS EQUAL TO OR LARGER THAN 1000).
301 C METHOD UTILIZED--SHEFFE-TUKEY APPROXIMATION
302 C (SEE JOHNSON AND KOTZ, VOLUME 2, PAGE 84, THIRD FORMULA).
303 C
304 C CONTINUE
305 TERM1=DNU1
306 TERM2=(DNU1/DNU2)*(0.5D0*DNU1-1.0D0)
307 TERM3=-(DNU1/DNU2)*0.5D0
308 U=(TERM1+TERM2)/((1.0D0/DX-TERM3)
309 CALL CHSCDF (U,NU1,CCDF)
310 CDF=CCDF
311 RETURN
312
313 C TREAT THE CASE WHEN NU2 IS SMALL
314 C AND NU1 IS LARGE
315 C ( THAT IS, WHEN NU2 IS SMALLER THAN 100,
316 C AND NU1 IS EQUAL TO OR LARGER THAN 1000).
317 C METHOD UTILIZED--SHEFFE-TUKEY APPROXIMATION
318 C (SEE JOHNSON AND KOTZ, VOLUME 2, PAGE 84, THIRD FORMULA).
319 C
320 C CONTINUE
321 TERM1=DNU2
322 TERM2=(DNU2/DNU1)*(0.5D0*DNU2-1.0D0)
323 TERM3=-(DNU2/DNU1)*0.5D0
324 U=(TERM1+TERM2)/(DX-TERM3)
325 CALL CHSCDF (U,NU2,CCDF)
326 CDF=1.0-CCDF
327 RETURN
328 C
329

```

1 C SUBROUTINE FPPF (P, NU1, NU2, PPF)
 2 C
 3 C PURPOSE--THIS SUBROUTINE COMPUTES THE PERCENT POINT
 4 C FOR THE F DISTRIBUTION
 5 C WITH INTEGER DEGREES OF FREEDOM
 6 C PARAMETERS = NU1 AND NU2.
 7 C THIS DISTRIBUTION IS DEFINED FOR ALL NON-NEGATIVE X.
 8 C THE PROBABILITY DENSITY FUNCTION IS GIVEN
 9 C IN THE REFERENCES BELOW.
 10 C INPUT ARGUMENTS--P = THE SINGLE PRECISION VALUE
 11 C (BETWEEN 0.0 AND 1.0),
 12 C AT WHICH THE PERCENT POINT
 13 C FUNCTION IS TO BE EVALUATED.
 14 C --NU1 = THE INTEGER DEGREES OF FREEDOM
 15 C FOR THE NUMERATOR OF THE F RATIO.
 16 C NU1 SHOULD BE POSITIVE.
 17 C --NU2 = THE INTEGER DEGREES OF FREEDOM
 18 C FOR THE DENOMINATOR OF THE F RATIO.
 19 C NU2 SHOULD BE POSITIVE.
 20 C OUTPUT ARGUMENTS--PPF = THE SINGLE PRECISION PERCENT POINT
 21 C FUNCTION VALUE.
 22 C OUTPUT--THE SINGLE PRECISION PERCENT POINT
 23 C FUNCTION VALUE PPF FOR THE F DISTRIBUTION
 24 C WITH DEGREES OF FREEDOM
 25 C PARAMETERS = NU1 AND NU2.
 26 C PRINTING--NONE UNLESS AN INPUT ARGUMENT ERROR CONDITION EXISTS.
 27 C RESTRICTIONS--P SHOULD BE BETWEEN
 28 C 0.0 (INCLUSIVELY) AND 1.0 (EXCLUSIVELY).
 29 C --NU1 SHOULD BE A POSITIVE INTEGER VARIABLE.
 30 C --NU2 SHOULD BE A POSITIVE INTEGER VARIABLE.
 31 C OTHER DATAPAC SUBROUTINES NEEDED--FCDF, NORCDF, CHSCDF, NORPPF.
 32 C FORTRAN LIBRARY SUBROUTINES NEEDED--DSQRT, DATAN.
 33 C MODE OF INTERNAL OPERATIONS--DOUBLE PRECISION.
 34 C LANGUAGE--ANSI FORTRAN.
 35 C REFERENCES--NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS
 36 C SERIES 55, 1964, PAGES 946-947,
 37 C FORMULAE 26.6.4, 26.6.5, 26.6.8, AND 26.6.15.
 38 C --JOHNSON AND KOTZ, CONTINUOUS UNIVARIATE
 39 C DISTRIBUTIONS--2, 1970, PAGE 63, FORMULA 20,
 40 C AND PAGE 84, THIRD FORMULA.
 41 C --PAULSON, AN APPROXIMATE NORMALIZATION
 42 C OF THE ANALYSIS OF VARIANCE DISTRIBUTION,
 43 C ANNALS OF MATHEMATICAL STATISTICS, 1942,
 44 C NUMBER 13, PAGES 233-135.
 45 C --SCHEFFE AND TUKEY, A FORMULA FOR SAMPLE SIZES
 46 C FOR POPULATION TOLERANCE LIMITS, 1944,
 47 C NUMBER 15, PAGE 217.
 48 C WRITTEN BY--JAMES J. FILLIBEN
 49 C STATISTICAL ENGINEERING LABORATORY (205.03)
 50 C NATIONAL BUREAU OF STANDARDS
 51 C WASHINGTON, D. C. 20234
 52 C PHONE: 301-921-2315
 53 C ORIGINAL VERSION--MAY 1978.
 54 C UPDATED --AUGUST 1979.
 55 C C-----
 56 C

1PR=6
59 C CHECK THE INPUT ARGUMENTS FOR ERRORS
60 C
61 C

FPPF0058
FPPF0059
FPPF0060
FPPF0061
FPPF0062
FPPF0063
FPPF0064
FPPF0065
FPPF0066
FPPF0067
FPPF0068
FPPF0069
FPPF0070
FPPF0071
FPPF0072
FPPF0073
FPPF0074
FPPF0075
FPPF0076
FPPF0077
FPPF0078
FPPF0079
FPPF0080
FPPF0081
FPPF0082
FPPF0083
FPPF0084
FPPF0085
FPPF0086
FPPF0087
FPPF0088
FPPF0089
FPPF0090
FPPF0091
FPPF0092
FPPF0093
FPPF0094
FPPF0095
FPPF0096
FPPF0097
FPPF0098
FPPF0099
FPPF0100
FPPF0101
FPPF0102
FPPF0103
FPPF0104
FPPF0105
FPPF0106
FPPF0107
FPPF0108
FPPF0109
FPPF0110
FPPF0111
FPPF0112
FPPF0113
FPPF0114
FPPF0115

PPF=0.0
IF (NU1.LE.0) GO TO 10
IF (NU2.LE.0) GO TO 20
IF (P.LT.0.0.OR.P.GE.1.0) GO TO 30
GO TO 40
WRITE (IPR,60)
WRITE (IPR,90) NU1
PPF=0.0
RETURN
20 WRITE (IPR,70)
WRITE (IPR,90) NU2
PPF=0.0
RETURN
30 WRITE (IPR,50)
WRITE (IPR,80) P
PPF=0.0
RETURN
40 CONTINUE
FORMAT (1H,1I3H***** FATAL ERROR--THE FIRST INPUT ARGUMENT TO THFPPF0080
2E FPPF SUBROUTINE IS OUTSIDE THE ALLOWABLE (0,1) INTERVAL *****)
81 60 FORMAT (1H,9I1H***** FATAL ERROR--THE SECOND INPUT ARGUMENT TO THFPPF0081
2 FPPF SUBROUTINE IS NON-POSITIVE *****)
83 70 FORMAT (1H,9I1H***** FATAL ERROR--THE THIRD INPUT ARGUMENT TO THFPPF0082
2 FCDF SUBROUTINE IS NON-POSITIVE *****)
85 80 FORMAT (1H,35H***** THE VALUE OF THE ARGUMENT IS ,E15.8,6H *****)
86 90 FORMAT (1H,35H***** THE VALUE OF THE ARGUMENT IS ,18,6H *****)
87 90 FORMAT (1H,35H***** THE VALUE OF THE ARGUMENT IS ,18,6H *****)
88 C-----START POINT-----
90 C
91 C IBUG=0.0
92 C TOL=0.0000001
93 C MAXIT=100
94 C XMIN=0.0
95 C XMAX=10.0***30
96 C XLOW=XMIN
97 C XUP=XMAX
98 C
99 C ANU1=NU1
ANU2=NU2
100 C
101 C EXPF=0.5*((1.0/ANU2)-(1.0/ANU1))
102 C SDF=SQRT(0.5*((1.0/ANU2)+(1.0/ANU1)))
103 C CALL NORPPF (P,ZN)
104 C XN=EXPF+ZN*SDF
105 C XMID=EXP(2.0*XN)
106 C
107 C IF (IBUG.EQ.1) WRITE (6,100) XMID
108 C FORMAT (1H,7HXMID = ,E15.7)
109 C
110 C IF (P.EQ.0.0) GO TO 110
111 C GO TO 120
112 C
113 C CONTINUE
114 C PPF=XMIN
115 C
RETURN

```

116 120  CONTINUE
117  C      ICOUNT=0
118
119 130  CONTINUE
120  X=XMIN
121  CALL FCDF (X,NU1,NU2,PCALC)
122  IF (PCALC.EQ.P) GO TO 190
123  IF (PCALC.GT.P) GO TO 160
124
125 140  CONTINUE
126  XLOW=XMIN
127
128  X=XMIN/2.0
129  IF (X.GE.XUP) GO TO 150
130  XMID=X
131  IF (IBUG.EQ.1) WRITE (6,100) XMID
132  CALL FCDF (X,NU1,NU2,PCALC)
133  IF (PGALC.EQ.P) GO TO 190
134  IF (PCALC.LT.P) GO TO 140
135  XUP=X
136
137  XMID=(XLOW+XUP)/2.0
138  IF (IBUG.EQ.1) WRITE (6,100) XMID
139  GO TO 180
140
141 160  CONTINUE
142  XUP=XMIN
143  X=XMIN/2.0
144  IF (X.LE.XLOW) GO TO 170
145  XMID=X
146  IF (IBUG.EQ.1) WRITE (6,100) XMID
147  CALL FCDF (X,NU1,NU2,PCALC)
148  IF (PGALC.EQ.P) GO TO 190
149  IF (PCALC.GT.P) GO TO 160
150  XLOW=X
151
152  XMID=(XLOW+XUP)/2.0
153  IF (IBUG.EQ.1) WRITE (6,100) XMID
154  GO TO 180
155
156 180  CONTINUE
157  XDEL=ABS(XMID-XLOW)
158  ICOUNT=ICOUNT+1
159  IF (XDEL.LT.TOL.OR.ICOUNT.GT.MAXIT) GO TO 190
160  GO TO 130
161
162 190  CONTINUE
163  PPF=XMID
164
165  C      RETURN
166  END

```

CPP*NS(1) . GETX(2) SUBROUTINE GETX (XF, YF, NF, Y, L, M, X, I, KS, KL)

```
1      C-----  
2      C-----  
3      C      GETX      WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING  
4      C      DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.  
5      C      AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION  
6      C      FOR: THE INVERSE INTERPOLATION OF A CALIBRATION CURVE OR ITS  
7      C      UPPER OR LOWER CONFIDENCE LIMIT WHEREBY AN X-VALUE IS  
8      C      COMPUTED FOR A GIVEN Y-VALUE  
9      C      SUBPROGRAMS CALLED: -NONE-  
10     C      CURRENT VERSION COMPLETED JUNE 18, 1980  
11     C-----  
12     DIMENSION XF(NF), YF(NF)  
13     IF (Y,LT,XF(L+1)) GO TO 20  
14     IF (L+1, EQ, NF) GO TO 30  
15     L=L+1  
16     GO TO 10  
17     IF (L, EQ, 0) GO TO 40  
18     C=(Y-YF(L))/(YF(L+1)-YF(L))  
19     X=C*(XF(L+1)-XF(L))+XF(L)  
20     I=1  
21     RETURN  
22     X=XF(NF)  
23     I=(5+MD)/2  
24     KL=KL+1  
25     RETURN  
26     X=XF(1)  
27     I=(5-MD)/2  
28     KS=KS+1  
29     RETURN  
30     END
```

CPR*NS(1) .INTERV(1)

1 SUBROUTINE INTERV (XT,LXT,X,LEFT,MFLAG)
 2 C FROM * A PRACTICAL GUIDE TO SPLINES * BY C. DE BOOR
 3 COMPUTES LEFT = MAX(1 , 1 .LE. 1 .LE. LXT .AND. XT(1) .LE. X) .
 4 C
 5 C***** I N P U T *****
 6 C XT.....A REAL SEQUENCE, OF LENGTH LXT , ASSUMED TO BE NONDECREASING
 7 C LXT.....NUMBER OF TERMS IN THE SEQUENCE XT
 8 C X.....THE POINT WHOSE LOCATION WITH RESPECT TO THE SEQUENCE XT IS
 9 C TO BE DETERMINED.
 10 C
 11 C***** O U T P U T *****
 12 C LEFT, MFLAG....BOTH INTEGERS, WHOSE VALUE IS
 13 C
 14 C 1 -1 IF XT(1) .LE. XT(1+1)
 15 C 1 0 IF XT(1) .LE. XT(1+1)
 16 C LXT 1 IF XT(LXT) .LE. X
 17 C
 18 C IN PARTICULAR, MFLAG = 0 IS THE 'USUAL' CASE. MFLAG .NE. 0
 19 C INDICATES THAT X LIES OUTSIDE THE HALFOPEN INTERVAL
 20 C XT(1) .LE. Y .LT. XT(LXT) . THE ASYMMETRIC TREATMENT OF THE
 21 C INTERVAL IS DUE TO THE DECISION TO MAKE ALL PP FUNCTIONS CONT-
 22 CINUOUS FROM THE RIGHT.
 23 C
 24 C***** M E T H O D *****
 25 C THE PROGRAM IS DESIGNED TO BE EFFICIENT IN THE COMMON SITUATION THAT
 26 C IT IS CALLED REPEATEDLY, WITH X TAKEN FROM AN INCREASING OR DECREASING
 27 C SING SEQUENCE. THIS WILL HAPPEN, E.G., WHEN A PP FUNCTION IS TO BE
 28 C GRAPHED. THE FIRST GUESS FOR LEFT IS THEREFORE TAKEN TO BE THE VAL-
 29 C UE RETURNED AT THE PREVIOUS CALL, AND STORED IN THE LOCAL VARIA-
 30 C BLE ILO . A FIRST CHECK ASCERTAINS THAT ILO .LT. LXT (THIS IS NEC-
 31 C ESSARY SINCE THE PRESENT CALL MAY HAVE NOTHING TO DO WITH THE PREVI-
 32 C OUS CALL) . THEN, IF XT(ILO) .LE. X .LT. XT(ILO+1) , WE SET LEFT =
 33 C ILO AND ARE DONE AFTER JUST THREE COMPARISONS
 34 C OTHERWISE, WE REPEATEDLY DOUBLE THE DIFFERENCE ISTEP = IHI - ILO
 35 C WHILE ALSO MOVING ILO AND IHI IN THE DIRECTION OF X , UNTIL
 36 C XT(ILO) .LE. X .LT. XT(IHI)
 37 C AFTER WHICH WE USE BISECTION TO GET, IN ADDITION, ILO+1 = IHI .
 38 C LEFT = ILO IS THEN RETURNED.
 39 C
 40 INTEGER LEFT,LXT,MFLAG,IHI,ILO,ISTEP,MIDDLE
 41 REAL X,XT(LXT)
 42 DATA ILO /1/
 43 C SAVE ILO (A VALID FORTRAN STATEMENT IN THE NEW 1977 STANDARD)
 44 C IHI=ILO+1
 45 IF (IHI .LT. LXT) GO TO 10
 46 IF (X.GE.XT(LXT)) GO TO 110
 47 IF (LXT.LE.1) GO TO 90
 48 ILO=LXT-1
 49 IHI=LXT
 50 C
 51 IF (X.GE.XT(IHI)) GO TO 40
 52 IF (X.GE.XT(ILO)) GO TO 100
 53 C
 54 C ISTEP=1
 55 IF (IHI=ILO) GO TO 100
 56 IF (ILO=IHI-ISTEP) GO TO 90
 57 C

```

58      IF ( ILO, LE, 1) GO TO 30
59      IF ( X, GE, XT( ILO)) GO TO 70
60      ISTEP=ISTEP*2
61      GO TO 20
62      ILO=1
63      IF ( X, LT, XT( 1)) GO TO 90
64      GO TO 70      *** NOW X .GE. XT( IHI) . INCREASE IHI TO CAPTURE X .
65      C
66      40      ISTEP=1
67      50      ILO= IHI
68      IHI= ILO+ISTEP
69      IF ( IHI, GE, LXT) GO TO 60
70      IF ( X, LT, XT( IHI)) GO TO 70
71      ISTEP=ISTEP*2
72      GO TO 50
73      IF ( X, GE, XT( LXT)) GO TO 110
74      IHI=LXT
75      C
76      C      *** NOW XT( ILO) .LE. X .LT. XT( IHI) . NARROW THE INTERVAL.
77      70      MIDDLE=( ILO+IHI)/2
78      IF ( MIDDLE, EQ, ILO) GO TO 100
79      C      NOTE. IT IS ASSUMED THAT MIDDLE = ILO IN CASE IHI = ILO+1 .
80      IF ( X, LT, XT( MIDDLE)) GO TO 80
81      ILO=MIDDLE
82      GO TO 70
83      IHI=MIDDLE
84      GO TO 70
85      C*** SET OUTPUT AND RETURN.
86      90      MFLAG=-1
87      LEFT=1
88      RETURN
89      MFLAG=0
90      LEFT= ILO
91      RETURN
92      110      MFLAG=1
93      LEFT=LXT
94      RETURN
95      END

```

```

CPR*NS(1) .L2APPR(1) SUBROUTINE L2APPR ( T, N, K, Q, DIAG, BCOEF, KMX, NPK, NTAU, TAU, GTAU,
1      2      2 WEIGHT)
2
3      C
4      INTEGER N, K, KMX, NPK, NTAU
5      REAL Q( KMX, N)
6      REAL T( NPK), DIAG( N), BCOEF( N), TAU( NTAU), GTAU( NTAU), WEIGHT( NTAU)
7
8      C CONSTRUCTS THE (WEIGHTED DISCRETE) L2-APPROXIMATION BY SPLINES OF ORDER N
9      C K WITH KNOT SEQUENCE T(1), . . . , T( N+K) TO GIVEN DATA POINTS
10     C ( TAU(1), GTAU(1) ), . . . , ( TAU( N), GTAU( N) ). THE B-SPLINE COEFFICIENTS
11     C B COEF OF THE APPROXIMATING SPLINE ARE DETERMINED FROM THE
12     C NORMAL EQUATIONS USING CHOLESKY'S METHOD.
13
14     C ON INPUT.
15
16     C T(*)          IS AN ARRAY OF SIZE AT LEAST NPK = N + K AND HOLDS
17     C THE KNOT SEQUENCE IN T(1) . . . T( NPK)
18
19     C N             IS THE DIMENSION OF THE SPACE OF SPLINES OF ORDER K
20
21     C K             IS THE ORDER OF THE SPLINES = DEGREE + 1
22
23     C Q(*, *)        IS A WORK ARRAY WITH ROW DIMENSION KMX AND COLUMN
24
25     C DIMENSION AT LEAST N.
26
27     C DIAG(*)        IS A WORK ARRAY OF SIZE AT LEAST N.
28
29     C KMX           IS THE ROW DIMENSION OF Q.
30
31     C NPK            IS N + K.
32
33     C NTAU           IS THE NUMBER OF DATA POINTS.
34
35     C TAU(*)         IS AN ARRAY OF SIZE AT LEAST NTAU WHICH CONTAINS
36     C THE ABSCISSAS OF THE DATA POINTS TO BE FITTED IN
37     C TAU(1) . . . TAU( NTAU).
38
39     C GTAU(*)        IS AN ARRAY OF SIZE AT LEAST NTAU WHICH CONTAINS
40     C THE ORDINATES OF THE DATA POINTS TO BE FITTED IN
41     C GTAU(1) . . . GTAU( NTAU).
42
43     C WEIGHT(*)      IS AN ARRAY OF SIZE AT LEAST NTAU WHICH CONTAINS
44     C THE CORRESPONDING WEIGHTS TO BE APPLIED TO THE
45     C DATA POINTS WHEN FITTING IN WEIGHT(1) . . .
46     C WEIGHT( NTAU) .
47
48     C ON OUTPUT.
49
50     C Q(*, *)        CONTAINS THE K LOWER DIAGONALS OF THE CHOLESKY
51     C FACTOR OF THE GRAMIAN MATRIX C IN ITS FIRST K ROWS.
52
53     C DIAG(*)        CONTAINS LITTLE OF IMPORTANCE.
54
55     C BCOEF(*)      IS AN ARRAY OF SIZE AT LEAST N WHICH CONTAINS THE N
56     C L2-APPROXIMATION IN B-SPLINE COEFFICIENTS OF THE L2 APPROXIMATION IN
57     C BCOEF(1) . . . BCOEF( N).

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58
59 C AND THE REST OF THE VARIABLES ARE UNCHANGED.
60 C *****
61 C THE B-SPLINE COEFFICIENTS OF THE L2-APPR. ARE DETERMINED AS THE SOL-
62 C UTION OF THE NORMAL EQUATIONS
63 C SUM ( (B(I),B(J))*BCOEF(J) : J=1,...,N) = (B(I),G),
64 C
65 C HERE, B(I) DENOTES THE I-TH B-SPLINE, G DENOTES THE FUNCTION TO
66 C BE APPROXIMATED, AND THE I N N E R P R O D U C T OF TWO FUNCT-
67 C IONS F AND G IS GIVEN BY
68 C (F,G) := SUM ( F(TAU(I))*G(TAU(I))*WEIGHT(I) : I=1,...,NTAU) .
69 C THE ARRAYS T A U AND W E I G H T ARE GIVEN IN COMMON BLOCK
70 C D A T A , AS IS THE ARRAY G T A U CONTAINING THE SEQUENCE
71 C G(TAU(I)), I=1,...,NTAU.
72 C THE RELEVANT FUNCTION VALUES OF THE B-SPLINES B(I), I=1,...,N, ARE
73 C SUPPLIED BY THE SUBPROGRAM B S P L V B .
74 C THE COEFF. MATRIX C, WITH
75 C C(I,J) := (B(I),B(J)), I, J=1,...,N,
76 C OF THE NORMAL EQUATIONS IS SYMMETRIC AND (2*K-1)-BANDED, THEREFORE
77 C CAN BE SPECIFIED BY GIVING ITS K BANDS AT OR BELOW THE DIAGONAL. FOR
78 C I=1,...,N, WE STORE
79 C (B(I),B(J)) = C(I,J) IN Q(I-J+1,J), J=I,...,MIN0(I+K-1,N)
80 C AND THE RIGHT SIDE
81 C (B(I),G) IN BCOEF(I)
82 C SINCE B-SPLINE VALUES ARE MOST EFFICIENTLY GENERATED BY FINDING SIM-
83 C ULTANEOUSLY THE VALUE OF EVERY NONZERO B-SPLINE AT ONE POINT,
84 C THE ENTRIES OF C (I.E., OF Q), ARE GENERATED BY COMPUTING, FOR
85 C EACH LL, ALL THE TERMS INVOLVING TAU(LL) SIMULTANEOUSLY AND ADDING
86 C THEM TO ALL RELEVANT ENTRIES.
87 C ADDITIONAL ROUTINES REQUIRED.
88 C
89 C
90 C BSPLVB BCHFAC BCHSLV
91 C
92 C MODIFICATION BY.
93 C
94 C MARTIN CORDES
95 C CENTER FOR APPLIED MATHEMATICS, NBS
96 C VERSION 1
97 C OCT 1979
98 C
99 C
100 C
101 C REAL BIATX(20)
102 C REAL DW
103 C INTEGER I,J,JJ,LEFT,LEFTMK,LL,MM
104 C FORMAT ('/5X,5H<<<14,1X,22HB-SPLINE COEFFICIENTS ,'
105 C 2 14HCOMPUTED >>>)
106 C
107 C DO 20 J=1,N
108 C BCOEF(J)=0
109 C DO 20 I=1,K
110 C Q(I,J)=0
111 C LEFT=K
112 C LEFTMK=0
113 C DO 50 LL=1,NTAU
114 C LOCATE LEFT S.T. TAU(LL) IN (T(LEFT),T(LEFT+1))L2APP115
115 C

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116 30 IF (LEFT.EQ.N) GO TO 40
117 IF (TAU(LL).LT.T(LEFT+1)) GO TO 40
118 LEFT=LEFT+1
119 LEFTMK=LEFTMK+1
120 GO TO 30
121 CALL BSPLVB (T,K,1,TAU(LL),LEFT,BIATX)
122 C BIATX(MM) CONTAINS THE VALUE OF B(LEFT-K+MM) AT TAU(LL).
123 C HENCE, WITH DW := BIATX(MM)*WEIGHT(LL), THE NUMBER DW*CTAU(LL)
124 C IS A SUMMAND IN THE INNER PRODUCT
125 C (B(LEFT-K+MM), G) WHICH GOES INTO BCOEF(LEFT-K+MM)
126 C AND THE NUMBER BIATX(JJ)*DW IS A SUMMAND IN THE INNER PRODUCT
127 C (B(LEFT-K+JJ), B(LEFT-K+MM)), INTO Q(JJ-MM+1,LEFT-K+MM)
128 C SINCE (LEFT-K+JJ) - (LEFT-K+MM) + 1 = JJ - MM + 1 .
129 DO 50 MM=1,K
130 DW=BIATX(MM)*WEIGHT(LL)
131 J=LEFTMK+MM
132 BCOEF(J)=DW*CTAU(LL)+BCOEF(J)
133 I=1
134 DO 50 JJ=MM,K
135 Q(I,J)=BIATX(JJ)*DW+Q(I,J)
136 I=I+1
137 C
138 C CONSTRUCT CHOLESKY FACTORIZATION FOR C IN Q, THEN USE L2APP138
139 C IT TO SOLVE THE NORMAL EQUATIONS L2APP139
140 C G*X = BCOEF L2APP140
141 C FOR X, AND STORE X IN BCOEF L2APP141
142 CALL BCHFAC (Q,KTX,K,N,DIAG) L2APP142
143 CALL BCHSLV (Q,KTX,K,N,BCOEF) L2APP143
144 WRITE (*,10) N L2APP144
145 RETURN L2APP145
146 END L2APP146

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CPR*NS(1) . NORCDF(1) . SUBROUTINE NORCDF ( X, CDF)
1      C NORCDF01
2      C NORCDF02
3      C NORCDF03
4      C NORCDF04
5      C NORCDF05
6      C NORCDF06
7      C NORCDF07
8      C NORCDF08
9      C NORCDF09
10     C NORCDF10
11     C NORCDF11
12     C NORCDF12
13     C NORCDF13
14     C NORCDF14
15     C NORCDF15
16     C NORCDF16
17     C NORCDF17
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51     C NORCDF51
52     C NORCDF52
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54     C NORCDF54
55     C NORCDF55
56     C NORCDF56

C PURPOSE--THIS SUBROUTINE COMPUTES THE CUMULATIVE DISTRIBUTION
C FUNCTION VALUE FOR THE NORMAL (GAUSSIAN)
C DISTRIBUTION WITH MEAN = 0 AND STANDARD DEVIATION = 1.
C THIS DISTRIBUTION IS DEFINED FOR ALL X AND HAS
C THE PROBABILITY DENSITY FUNCTION
C  $F(X) = (1/SQRT(2*pi)) * EXP(-X*X/2).$ 
C INPUT  ARGUMENTS--X = THE SINGLE PRECISION VALUE AT
C WHICH THE CUMULATIVE DISTRIBUTION
C FUNCTION IS TO BE EVALUATED.
C OUTPUT ARGUMENTS--CDF = THE SINGLE PRECISION CUMULATIVE
C DISTRIBUTION FUNCTION VALUE CDF.
C OUTPUT--THE SINGLE PRECISION CUMULATIVE DISTRIBUTION
C PRINTING--NONE.
C RESTRICTIONS--NONE.
C OTHER DATAPAC SUBROUTINES NEEDED--NONE.
C FORTRAN LIBRARY SUBROUTINES NEEDED--EXP.
C MODE OF INTERNAL OPERATIONS--SINGLE PRECISION.
C LANGUAGE--ANSI FORTRAN.
C REFERENCES--NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS
C SERIES 55, 1964, PAGE 932, FORMULA 26.2, 17.
C --JOHNSON AND KOTZ, CONTINUOUS UNIVARIATE
C DISTRIBUTIONS--1, 1970, PAGES 40-111.
C WRITTEN BY--JAMES J. FILLIBEN
C STATISTICAL ENGINEERING LABORATORY (205.03)
C NATIONAL BUREAU OF STANDARDS
C WASHINGTON, D. C. 20234
C PHONE: 301-921-2315
C ORIGINAL VERSION--JUNE 1972.
C UPDATED --SEPTEMBER 1975.
C UPDATED --NOVEMBER 1975.

C-----DATA B1,B2,B3,B4,B5,P/.319381530,-0.356563782,1.781477937,
C-----2 -1.821255978,1.330274429,.2316419,/
C-----IPR=6
C-----START POINT-----
C-----Z=X
C-----IF (X.LT.0.0) Z=-Z
C-----T=1.0/(1.0+P*Z)
C-----CDF=1.0-((0.39894228040143)*EXP(-0.5*Z*Z))*(B1*T+B2*T*T+B3*T*T*T+B4*T*T*T*T)
C-----24*T*T*T*B5*T*T*T*T
C-----IF (X.LT.0.0) CDF=1.0-CDF
C-----RETURN
C-----END

```

1 C NORPPF(1). NORPPF (P,PPF)
 2 C
 3 C PURPOSE-- THIS SUBROUTINE COMPUTES THE PERCENT POINT
 4 C FUNCTION VALUE FOR THE NORMAL (GAUSSIAN)
 5 C DISTRIBUTION WITH MEAN = 0 AND STANDARD DEVIATION = 1.
 6 C THIS DISTRIBUTION IS DEFINED FOR ALL X AND HAS
 7 C THE PROBABILITY DENSITY FUNCTION
 8 C $f(x) = (1/\sqrt{2\pi}) * \exp(-x^2/2)$.
 9 C NOTE THAT THE PERCENT POINT FUNCTION OF A DISTRIBUTION
 10 C IS IDENTICALLY THE SAME AS THE INVERSE CUMULATIVE
 11 C DISTRIBUTION FUNCTION OF THE DISTRIBUTION.
 12 C INPUT ARGUMENTS--P = THE SINGLE PRECISION VALUE
 13 C (BETWEEN 0.0 AND 1.0)
 14 C AT WHICH THE PERCENT POINT
 15 C FUNCTION IS TO BE EVALUATED.
 16 C OUTPUT ARGUMENTS--PPF = THE SINGLE PRECISION PERCENT
 17 C POINT FUNCTION VALUE.
 18 C OUTPUT--THE SINGLE PRECISION PERCENT POINT
 19 C FUNCTION VALUE PPF.
 20 C PRINTING--NONE UNLESS AN INPUT ARGUMENT ERROR CONDITION EXISTS.
 21 C RESTRICTIONS--P SHOULD BE BETWEEN 0.0 AND 1.0, EXCLUSIVELY.
 22 C OTHER DATA¹AC SUBROUTINES NEEDED--NONE.
 23 C FORTRAN LIBRARY SUBROUTINES NEEDED--SQRT, ALOG.
 24 C MODE OF INTERNAL OPERATIONS--SINGLE PRECISION.
 25 C LANGUAGE--ANSI FORTRAN.
 26 C REFERENCES--ODEH AND EVANS, THE PERCENTAGE POINTS
 27 C OF THE NORMAL DISTRIBUTION, ALGORITHM 70,
 28 C APPLIED STATISTICS, 1974, PAGES 96-97.
 29 C --EVANS, ALGORITHMS FOR MINIMAL DEGREE
 30 C POLYNOMIAL AND RATIONAL APPROXIMATION,
 31 C M. SC. THESIS, 1972, UNIVERSITY
 32 C OF VICTORIA, B. C., CANADA.
 33 C --HASTINGS, APPROXIMATIONS FOR DIGITAL
 34 C COMPUTERS, 1955, PAGES 113, 191, 192.
 35 C --NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS
 36 C SERIES 55, 1964, PAGE 933, FORMULA 26.2.23.
 37 C --FILIBEN, SIMPLE AND ROBUST LINEAR ESTIMATION
 38 C OF THE LOCATION PARAMETER OF A SYMMETRIC
 39 C DISTRIBUTION (UNPUBLISHED PH.D. DISSERTATION,
 40 C PRINCETON UNIVERSITY), 1969, PAGES 21-44, 229-231.
 41 C --FILIBEN, 'THE PERCENT POINT FUNCTION',
 42 C (UNPUBLISHED MANUSCRIPT), 1970, PAGES 28-31.
 43 C --JOHNSON AND KOTZ, CONTINUOUS UNIVARIATE
 44 C DISTRIBUTIONS--1, 1970, PAGES 40-111.
 45 C --THE KELLEY STATISTICAL TABLES, 1948.
 46 C --OWEN, HANDBOOK OF STATISTICAL TABLES,
 47 C 1962, PAGES 3-16.
 48 C --PEARSON AND HARTLEY, BIOMETRIKA TABLES
 49 C FOR STATISTICIANS, VOLUME 1, 1954,
 50 C PAGES 104-113.
 51 C COMMENTS--THE CODING AS PRESENTED BELOW
 52 C IS ESSENTIALLY IDENTICAL TO THAT
 53 C PRESENTED BY ODEH AND EVANS
 54 C AS ALGORITHM 70 OF APPLIED STATISTICS.
 55 C THE PRESENT AUTHOR HAS MODIFIED THE
 56 C ORIGINAL ODEH AND EVANS CODE WITH ONLY
 57 C MINOR STYLISTIC CHANGES.

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--AS POINTED OUT BY ODEH AND EVANS
--IN APPLIED STATISTICS.
--THEIR ALGORITHM REPRESENTS A
--SUBSTANTIAL IMPROVEMENT OVER THE
--PREVIOUSLY EMPLOYED
--HASTINGS APPROXIMATION FOR THE
--NORMAL PERCENT POINT FUNCTION--
--THE ACCURACY OF APPROXIMATION
--BEING IMPROVED FROM  $4.5 * (10^{-4})$ 
--TO  $1.5 * (10^{-8})$ .
--WRITTEN BY--JAMES J. FILLIBEN
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--WASHINGTON, D. C. 20234
--PHONE: 301-921-2315
--ORIGINAL VERSION--JUNE 1972.
--UPDATED --SEPTEMBER 1975.
--UPDATED --NOVEMBER 1975.
--UPDATED --OCTOBER 1976.

-----  

DATA P0,P1,P2,P3,P4 /-.322232431088,-1.0, -.3422420088547,
2 -.204231210245E-1, -.453642210148E-4/
DATA Q0,Q1,Q2,Q3,Q4 /.993484626060E-1, .588581570495, .531103462366,
2 .103537752856, .385660700634E-2/  

C
C IPR=6
C
C CHECK THE INPUT ARGUMENTS FOR ERRORS
C
C IF (P.LE.0.0.OR.P.GE.1.0) GO TO 10
C GO TO 20
C WRITE (IPR,30)
C WRITE (IPR,40) P
C RETURN
C
C CONTINUE
C FORMAT (1H,'115H**** FATAL ERROR--THE FIRST INPUT ARGUMENT TO THNORPP095
2E NORPP SUBROUTINE IS OUTSIDE THE ALLOWABLE (0,1) INTERVAL *****) NORPP096
FORMAT (1H,'35H**** THE VALUE OF THE ARGUMENT IS ,E15.8,6H *****) NORPP097
C
C-----START POINT-----
C
C IF (P.NE.0.5) GO TO 50
C
C IF (P.GT.0.5) R=1.0-R
C T=SQRT(-2.0*ALOG(R))
C ANUM=((((T*P4+Q3)*T+P2)*T+P1)*T+P0)
C ADEN=((((T*Q4+Q3)*T+Q2)*T+Q1)*T+Q0)
C PPF=T+(ANUM/ADEN)
C IF (P.LT.0.5) PPF=-PPF
C RETURN
C
C R=P
C IF (P.GT.0.5) R=1.0-R
C T=SQRT(-2.0*ALOG(R))
C ANUM=((((T*P4+P3)*T+P2)*T+P1)*T+P0)
C ADEN=((((T*Q4+Q3)*T+Q2)*T+Q1)*T+Q0)
C PPF=T+(ANUM/ADEN)
C IF (P.LT.0.5) PPF=-PPF
C RETURN
C
C END

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PURPOSE--THIS SUBROUTINE YIELDS A ONE-PAGE PRINTER PLOT
 OF Y(I) VERSUS X(I) WITH SPECIAL PLOTTING
 CHARACTERS.
 THIS 'SPECIAL PLOTTING CHARACTER' CAPABILITY
 ALLOWS THE DATA ANALYST TO INCORPORATE INFORMATION
 FROM A THIRD VARIABLE (ASIDE FROM Y AND X) INTO
 THE PLOT.
 THE PLOT CHARACTER USED AT THE I-TH PLOTTING
 POSITION (THAT IS, AT THE COORDINATE (X(I),Y(I)))
 WILL BE
 1 IF CHAR(I) IS BETWEEN 0.5 AND 1.5
 2 IF CHAR(I) IS BETWEEN 1.5 AND 2.5
 .
 .
 .
 9 IF CHAR(I) IS BETWEEN 8.5 AND 9.5
 . IF CHAR(I) IS BETWEEN 9.5 AND 10.5
 A IF CHAR(I) IS BETWEEN 10.5 AND 11.5
 B IF CHAR(I) IS BETWEEN 11.5 AND 12.5
 C IF CHAR(I) IS BETWEEN 12.5 AND 13.5
 .
 .
 W IF CHAR(I) IS BETWEEN 32.5 AND 33.5
 X IF CHAR(I) IS BETWEEN 33.5 AND 34.5
 Y IF CHAR(I) IS BETWEEN 34.5 AND 35.5
 Z IF CHAR(I) IS BETWEEN 35.5 AND 36.5
 X IF CHAR(I) IS ANY VALUE OUTSIDE THE RANGE
 0.5 TO 36.5.
 INPUT ARGUMENTS--Y = THE SINGLE PRECISION VECTOR OF
 (UNSORTED OR SORTED) OBSERVATIONS
 TO BE PLOTTED VERTICALLY.
 --X = THE SINGLE PRECISION VECTOR OF
 (UNSORTED OR SORTED) OBSERVATIONS
 TO BE PLOTTED HORIZONTALLY.
 --CHAR = THE SINGLE PRECISION VECTOR OF
 OBSERVATIONS WHICH CONTROL THE
 VALUE OF EACH INDIVIDUAL PLOT
 CHARACTER.
 --N = THE INTEGER NUMBER OF OBSERVATIONS
 IN THE VECTOR Y.
 OUTPUT--A ONE-PAGE PRINTER PLOT OF Y(I) VERSUS X(I)
 WITH SPECIAL PLOT CHARACTERS.
 PRINTING--YES.
 RESTRICTIONS--THERE IS NO RESTRICTION ON THE MAXIMUM VALUE
 OF N FOR THIS SUBROUTINE.
 OTHER DATAPAC SUBROUTINES NEEDED--NONE.
 FORTAN LIBRARY SUBROUTINES NEEDED--NONE.
 MODE OF INTERNAL OPERATIONS--SINGLE PRECISION.
 LANGUAGE--ANSI FORTRAN.
 COMMENT--VALUES IN THE VERTICAL AXIS VECTOR (Y),
 THE HORIZONTAL AXIS VECTOR (X),
 OR THE PLOT CHARACTER VECTOR (CHAR) WHICH ARE
 EQUAL TO OR IN EXCESS OF 10.***10 WILL NOT BE
 PLOTTED.

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THIS CONVENTION CREATLY SIMPLIFIES THE PROBLEM
 OF PLOTTING WHEN SOME ELEMENTS IN THE VECTOR Y
 (OR X, OR CHAR) ARE 'MISSING DATA', OR WHEN WE PURPOSELY
 WANT TO IGNORE CERTAIN ELEMENTS IN THE VECTOR Y
 (OR X, OR CHAR) FOR PLOTTING PURPOSES (THAT IS, WE DO NOT PLOT)
 WANT CERTAIN ELEMENTS IN Y (OR X, OR CHAR) TO BE
 PLOTTED).

TO CAUSE SPECIFIC ELEMENTS IN Y (OR X, OR CHAR) TO BE
 IGNORED, WE REPLACE THE ELEMENTS BEFOREHAND
 (BY, FOR EXAMPLE, USE OF THE REPLIC SUBROUTINE)
 BY SOME LARGE VALUE (LIKE, SAY, 10.0**10) AND
 THEY WILL SUBSEQUENTLY BE IGNORED IN THE PLOT
 SUBROUTINE.

REFERENCES--JILLIBEN, 'STATISTICAL ANALYSIS OF INTERLAB
 FATIGUE TIME DATA', UNPUBLISHED MANUSCRIPT
 (AVAILABLE FROM AUTHOR)

PRESENTED AT THE 'COMPUTER-ASSISTED DATA
 ANALYSIS' SESSION AT THE NATIONAL MEETING
 OF THE AMERICAN STATISTICAL ASSOCIATION,
 NEW YORK CITY, DECEMBER 27-30, 1973.

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PHONE--301-921-2315
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 UPDATED --OCTOBER 1975.
 UPDATED --NOVEMBER 1975.
 UPDATED --FEBRUARY 1976.
 UPDATED --FEBRUARY 1977.
 MINOR UPDATES --APRIL 1980 BY CHARLES P. REEVE.

58 C PLOTC058
 59 C PLOTC059
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C
 2 ALPHAI(1),ALPHAI(2),ALPHAI(3),ALPHAI(4),ALPHAI(5),ALPHAI(6),
 3 ALPHAI(1),ALPHAI(2),ALPHAI(3),ALPHAI(4),ALPHAI(5),ALPHAI(6),
 4 ALPHAI(1),ALPHAI(2),ALPHAI(3),ALPHAI(4),ALPHAI(5),ALPHAI(6),
 5 ALPHAI(1),ALPHAI(2),ALPHAI(3),ALPHAI(4),ALPHAI(5),ALPHAI(6),
 6 1HL,1HO,1HT,1HC,1H,1HF,1HI,1HR,1HS,1HT,1H,1HS,1HE,1HC,1HO,1HN,
 7 1HD,1HT,1HH,1HI,1HR,1HD,1H,1HF,1HO,1HU,1HR,1HT,1HH/
 DATA BLANK,HYPHEN,ALPHAI,ALPHAX /1H,1H,1H,1H/
 DATA ALPHAM,ALPHAA,ALPHAD,ALPHAN,EQUAL /1HM,1HA,1HD,1HN,1H=/
 DATA IPLOT(1),IPLOT(2),IPLOT(3),IPLOT(4),IPLOT(5),IPLOT(6),
 2 IPLOT(7),IPLOT(8),IPLOT(9),IPLOT(10),IPLOT(11),IPLOT(12),
 3 IPLOT(13),IPLOT(14),IPLOT(15),IPLOT(16),IPLOT(17),IPLOT(18),IPLOT(19),IPLOT(20),IPLOT(21),IPLOT(22),IPLOT(23),IPLOT(24),IPLOT(25)

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5, IPLOT(25), IPLOT(26), IPLOT(27), IPLOT(28), IPLOT(29), IPLOT(30), IPLOT(31) 116
6, IPLOT(31), IPLOT(32), IPLOT(33), IPLOT(34), IPLOT(35), IPLOT(36), IPLOT(37) 117
7, IPLOT(37) / 1H1, 1H2, 1H3, 1H4, 1H5, 1H6, 1H7, 1H8, 1H9, 1H, '1HA, 1HB, 1HC, 118
8 1HD, 1HE, 1HF, 1HG, 1HH, 1HI, 1HJ, 1HK, 1HL, 1HM, 1HN, 1HO, 1HP, 1HQ, 1HS, 119
9 1HT, 1HU, 1HV, 1HW, 1HY, 1HZ, 1HK/ 120
121
122 IPR=6
123 CUTOFF=(10.0**10)-1000.0
124 C
125 C CHECK THE INPUT ARGUMENTS FOR ERRORS
126 C
127 IF (ITYPE.EQ.1) WRITE (IPR,520)
128 IF (ITYPE.EQ.2) WRITE (IPR,530)
129 IF (N.LT.1) GO TO 10
130 GO TO 20
131 WRITE (IPR,200)
132 WRITE (IPR,210)
133 WRITE (IPR,230) (ALPHA4(L), L=1,6), (SBNAME(L), L=1,6)
134 WRITE (IPR,260) N
135 WRITE (IPR,200)
136 RETURN
137 CONTINUE
138 IF (N.EQ.1) GO TO 30
139 GO TO 40
140 WRITE (IPR,200)
141 WRITE (IPR,210)
142 WRITE (IPR,230) (ALPHA4(L), L=1,6), (SBNAME(L), L=1,6)
143 WRITE (IPR,270) N
144 WRITE (IPR,200)
145 RETURN
146 CONTINUE
147 C
148 HOLD=Y(1)
149 DO 50 I=2,N
150 IF (Y(I).NE. HOLD) GO TO 60
151 CONTINUE
152 WRITE (IPR,200)
153 WRITE (IPR,210)
154 WRITE (IPR,230) (ALPHA1(L), L=1,6), (SBNAME(L), L=1,6)
155 WRITE (IPR,280) HOLD
156 WRITE (IPR,200)
157 RETURN
158 CONTINUE
159 HOLD=X(1)
160 DO 70 I=2,N
161 IF (X(I).NE. HOLD) GO TO 80
162 CONTINUE
163 WRITE (IPR,200)
164 WRITE (IPR,210)
165 WRITE (IPR,230) (ALPHA2(L), L=1,6), (SBNAME(L), L=1,6)
166 WRITE (IPR,280) HOLD
167 WRITE (IPR,200)
168 RETURN
169 CONTINUE
170 HOLD=CHAR(1)
171 DO 90 I=2,N
172 IF (CHAR(I).NE. HOLD) GO TO 100
173 CONTINUE

```

```

174      WRITE ( IPR, 200)
175      WRITE ( IPR, 220)
176      WRITE ( IPR, 230) ( ALPHA3(L) , L=1, 6) , ( SBNAM(E(L) , L=1, 6)
177      WRITE ( IPR, 280) HOLD
178      WRITE ( IPR, 200)
179      CONTINUE
180
C      DO 110 I=1,N
181      IF ( Y(I) .LT. CUTOFF) GO TO 120
182      CONTINUE
183
184      WRITE ( IPR, 200)
185      WRITE ( IPR, 210)
186      WRITE ( IPR, 230) ( ALPHA1(L) , L=1, 6) , ( SBNAM(E(L) , L=1, 6)
187      WRITE ( IPR, 290)
188      WRITE ( IPR, 300) CUTOFF
189      WRITE ( IPR, 200)
190      RETURN
191      CONTINUE
192      DO 130 I=1,N
193      IF ( X(I) .LT. CUTOFF) GO TO 140
194      CONTINUE
195      WRITE ( IPR, 200)
196      WRITE ( IPR, 210)
197      WRITE ( IPR, 230) ( ALPHA2(L) , L=1, 6) , ( SBNAM(E(L) , L=1, 6)
198      WRITE ( IPR, 290)
199      WRITE ( IPR, 300) CUTOFF
200      WRITE ( IPR, 200)
201      RETURN
202      CONTINUE
203      DO 150 I=1,N
204      IF ( CHAR( I) .LT. CUTOFF) GO TO 160
205      CONTINUE
150
206      WRITE ( IPR, 200)
207      WRITE ( IPR, 210)
208      WRITE ( IPR, 230) ( ALPHA3(L) , L=1, 6) , ( SBNAM(E(L) , L=1, 6)
209      WRITE ( IPR, 290)
210      WRITE ( IPR, 300) CUTOFF
211      WRITE ( IPR, 200)
212      RETURN
213      CONTINUE
214      N2=0
215      DO 180 I=1,N
216      IF ( Y(I) .LT. CUTOFF .AND. X(I) .LT. CUTOFF .AND. CHAR( I) .LT. CUTOFF) GO TO 217
217      2 170
218      GO TO 180
219      N2=N2+1
220      IF ( N2.GE. 2) GO TO 190
221      CONTINUE
222      WRITE ( IPR, 200)
223      WRITE ( IPR, 210)
224      WRITE ( IPR, 240) ( ALPHA1(L) , L=1, 6) , ( ALPHA2(L) , L=1, 6) , ( ALPHA3(L) , L=1, 6)
225      2,6)
226      WRITE ( IPR, 250) ( SBNAM(E(L) , L=1, 6)
227      WRITE ( IPR, 310)
228      WRITE ( IPR, 320) N2
229      WRITE ( IPR, 200)
230      RETURN

```

```

CONTINUE
190
C 200  FORMAT (1H , 50H*****)
C 201  2 20H*****)
C 202  FORMAT (1H , 50H*****)
C 203  FATAL ERROR
C 204  NON-FATAL DIAGNOSTIC
C 205  INPUT ARGUMENT TO THE ,6A1.
C 206  2 1H SUBROUTINE)
C 207  FORMAT (1H , 4HTHE ,6A1 ,2H, '6A1,6H, AND ,6A1)
C 208  FORMAT (1H , 50H*****)
C 209  FORMAT (1H , 4HTHE ,6A1 ,23H INPUT ARGUMENT TO THE ,6A1,
C 210  FORMAT (1H , 50H*****)
C 211  2 1H SUBROUTINE)
C 212  FORMAT (1H , 4HTHE ,6A1 ,2H, '6A1,6H, AND ,6A1)
C 213  FORMAT (1H , 50H*****)
C 214  FORMAT (1H , 30H HIS NON-NEGATIVE (WITH VALUE = ,1B ,1H )
C 215  FORMAT (1H , 15H HAS THE VALUE 1)
C 216  FORMAT (1H , 19H HAS ALL ELEMENTS = ,E15.8)
C 217  FORMAT (1H , 40H HAS ALL ELEMENTS IN EXCESS OF THE CUTOFF)
C 218  FORMAT (1H , 9H VALUE OF ,E15.8)
C 219  FORMAT (1H , 39H ARE SUCH THAT TOO MANY POINTS HAVE BEEN,
C 220  FORMAT (1H , 5H ONLY ,I3 ,31H POINTS ARE LEFT TO BE PLOTTED.)
C 221  START POINT-----)
C 222
C 223  DETERMINE THE VALUES TO BE LISTED ON THE LEFT VERTICAL AXIS
C 224
C 225  DO 330 I=1,N
C 226  IF (Y(I) .GE. CUTOFF) GO TO 330
C 227  IF (X(I) .GE. CUTOFF) GO TO 330
C 228  IF (CHAR(I) .GE. CUTOFF) GO TO 330
C 229  YMIN=Y(I)
C 230  YMAX=Y(I)
C 231  GO TO 340
C 232  CONTINUE
C 233  DO 350 I=1,N
C 234  IF (Y(I) .GE. CUTOFF) GO TO 350
C 235  IF (X(I) .GE. CUTOFF) GO TO 350
C 236  IF (CHAR(I) .GE. CUTOFF) GO TO 350
C 237  YMIN=Y(I)
C 238  YMAX=Y(I)
C 239  GO TO 360
C 240  CONTINUE
C 241  DETERMINE THE VALUES TO BE LISTED ON THE BOTTOM HORIZONTAL AXIS
C 242  DETERMINE XMIN, XMAX, XMID, X25 (=THE 25% POINT) , AND
C 243  X75 (=THE 75% POINT)
C 244  DO 370 I=1,N
C 245  IF (Y(I) .GE. CUTOFF) GO TO 370
C 246  IF (X(I) .GE. CUTOFF) GO TO 370
C 247  IF (CHAR(I) .GE. CUTOFF) GO TO 370
C 248  XMIN=X(I)
C 249  XMAX=X(I)
C 250  GO TO 380
C 251  CONTINUE
C 252
C 253  DETERMINE THE VALUES TO BE LISTED ON THE LEFT VERTICAL AXIS
C 254
C 255  DO 330 I=1,N
C 256  IF (Y(I) .GE. CUTOFF) GO TO 330
C 257  IF (X(I) .GE. CUTOFF) GO TO 330
C 258  IF (CHAR(I) .GE. CUTOFF) GO TO 330
C 259  YMIN=Y(I)
C 260  YMAX=Y(I)
C 261  GO TO 340
C 262  CONTINUE
C 263  DO 350 I=1,N
C 264  IF (Y(I) .GE. CUTOFF) GO TO 350
C 265  IF (X(I) .GE. CUTOFF) GO TO 350
C 266  IF (CHAR(I) .GE. CUTOFF) GO TO 350
C 267  YMIN=Y(I)
C 268  YMAX=Y(I)
C 269  GO TO 360
C 270  CONTINUE
C 271  AIM1=I-1
C 272  YTABLE(1)=YMAX-(AIM1/8.0)*(YMAX-YMIN)
C 273  CONTINUE
C 274
C 275  DETERMINE THE VALUES TO BE LISTED ON THE BOTTOM HORIZONTAL AXIS
C 276  DETERMINE XMIN, XMAX, XMID, X25 (=THE 25% POINT) , AND
C 277  X75 (=THE 75% POINT)
C 278
C 279  DO 370 I=1,N
C 280  IF (Y(I) .GE. CUTOFF) GO TO 370
C 281  IF (X(I) .GE. CUTOFF) GO TO 370
C 282  IF (CHAR(I) .GE. CUTOFF) GO TO 370
C 283  XMIN=X(I)
C 284  XMAX=X(I)
C 285  GO TO 380
C 286  CONTINUE
C 287  DO 390 I=1,N
C 288  IF (Y(I) .GE. CUTOFF) GO TO 390
C 289  IF (X(I) .GE. CUTOFF) GO TO 390

```

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290
291      IF (CHAR(1).GE.CUTOFF) GO TO 390
292      IF (X(1).LT.XMIN) XMIN=X(1)
293      IF (X(1).GT.XMAX) XMAX=X(1)
294      CONTINUE
295      XMID=(XMIN+XMAX)/2.0
296      X25=0.75*XMIN+0.25*XMAX
297      X75=0.25*XMIN+0.75*XMAX
298      C      BLANK OUT THE GRAPH
299      C
300      DO 410 I=1,45
301      DO 400 J=1,109
302      IGRAPH(1,J)=BLANK
303      CONTINUE
304      410  CONTINUE
305      C      PRODUCE THE VERTICAL AXES
306      C
307      DO 420 I=3,43
308      IGRAPH(1,5)=ALPHAI
309      IGRAPH(1,109)=ALPHAI
310      CONTINUE
311      420  DO 430 I=3,43,5
312      IGRAPH(1,5)=HYPHEN
313      IGRAPH(1,5)=HYPHEN
314      IGRAPH(1,109)=HYPHEN
315      CONTINUE
316      IGRAPH(3,1)=EQUAL
317      IGRAPH(3,2)=ALPHAM
318      IGRAPH(3,3)=ALPHAA
319      IGRAPH(3,4)=ALPHAX
320      IGRAPH(23,1)=EQUAL
321      IGRAPH(23,2)=ALPHAM
322      IGRAPH(23,3)=ALPHAI
323      IGRAPH(23,4)=ALPHAD
324      IGRAPH(43,1)=EQUAL
325      IGRAPH(43,2)=ALPHAM
326      IGRAPH(43,3)=ALPHAI
327      IGRAPH(43,4)=ALPHAN
328      C      PRODUCE THE HORIZONTAL AXES
329      C
330      DO 440 J=7,107
331      IGRAPH(1,J)=HYPHEN
332      IGRAPH(45,J)=HYPHEN
333      CONTINUE
334      440  DO 450 J=7,107,25
335      IGRAPH(1,J)=ALPHAI
336      IGRAPH(45,J)=ALPHAI
337      CONTINUE
338      450  DO 460 J=20,107,25
339      IGRAPH(1,J)=ALPHAI
340      IGRAPH(45,J)=ALPHAI
341      CONTINUE
342      460  C      DETERMINE THE (X,Y) PLOT POSITIONS
343      C
344      C      RATIOY=40.0/(YMAX-YMIN)
345      C      RATIOX=100.0/(XMAX-XMIN)
346
347

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```

DO 470 I=1,N
  IF (Y(I) .GE. CUTOFF) GO TO 470
  IF (X(I) .GE. CUTOFF) GO TO 470
  IF (CHAR(I) .GE. CUTOFF) GO TO 470
  IF (CHAR(I) .LT. CUTOFF) GO TO 470
  MX=RATIO*(X(I)-XMIN)+0.5
  MX=MX+7
  MY=RATIO*(Y(I)-YMIN)+0.5
  MY=43-MY
  IARG=37
  IF (0.5 .LT. CHAR(I) .AND. CHAR(I) .LT. 36.5) IARG=CHAR(I)+0.5
  IGRAPH(MY, MX) = IPLOT(IARG)
  CONTINUE
  C   WRITE OUT THE GRAPH
 361  C
 362  C
 363  DO 480 I=1,45
 364    IP2=I+2
 365    IFLAG=IP2-(IP2/5)*5
 366    K=IP2/5
 367    IF (IFLAG.NE.0) WRITE (IPR,490) (IGRAPH(I,J),J=1,109)
 368    IF (IFLAG.EQ.0) WRITE (IPR,500) YTABLE(K),(IGRAPH(I,J),J=1,109)
 369    CONTINUE
 370    WRITE (IPR,510) XMIN, X25, XMID, X75, XMAX
 371    WRITE (IPR,540)
 372    C   FORMAT (1H ,20X,109A1)
 373    490  FORMAT (1H ,F20.7,109A1)
 374    500  FORMAT (1H ,14X,F20.7,5X,F20.7,1X,F20.7)
 375    510  FORMAT (1H ,59X,34HRESIDUALS VS. INDEPENDENT VARIABLE/)
 376    520  FORMAT (1H ,53X,47HSTANDARDIZED RESIDUALS VS. INDEPENDENT VARIABLE)
 377    530  FORMAT (1H ,53X,47HSTANDARDIZED RESIDUALS VS. INDEPENDENT VARIABLE)
 378    2//)
 379    540  FORMAT (//55X,44HKNOT LOCATIONS ARE INDICATED BY THE SYMBOL X)
 380    C   RETURN
 381    END
 382

```

CPR*NS(1) . PLOTSR(1)

PLOTSR1

```

1      SUBROUTINE PLOTSR (X, N, NX, HOR, RES, CHAR, NKX, T, K, KX)
2
3      C----- PLOTSR  WRITTEN BY CHARLES P. REEVE,  STATISTICAL ENGINEERING
4      C----- DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D. C.
5      C----- AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
6      C----- FOR: PLOTTING KNOT LOCATIONS AND RESIDUALS/STANDARDIZED RESIDUALS
7      C----- VS. INDEPENDENT VARIABLE
8      C----- SUBPROGRAMS CALLED: PLOTC
9      C----- CURRENT VERSION COMPLETED MARCH 14, 1980
10
11      C----- DIMENSION X(NX), HOR(NKX), RES(NKX), CHAR(NKX), T(NX)
12      C----- CREATE SUB-VECTORS OF INDEPENDENT VARIABLE AND STANDARDIZED
13      C----- RESIDUALS
14      DO 10 I=1,N
15      C----- SWITCH INDEPENDENT VARIABLE AND STANDARD DEVIATIONS OF RESIDUALS
16      Q=HOR(1)
17      HOR(1)=X(1)
18      XC(1)=Q
19      CHAR(1)=10.0
20      CONTINUE
21      C----- ADD KNOT LOCATIONS TO SUB-VECTORS
22      DO 20 I=1,K
23      L=I+N
24      BOR(L)=T(I)
25      RES(L)=0.0
26      CHAR(L)=0.0
27      CONTINUE
28      C----- GENERATE PLOT OF RESIDUALS VS. INDEPENDENT VARIABLE
29      NK=N+K
30      CALL PLOTC (RES, HOR, CHAR, NK, 1)
31      C----- CREATE SUB-VECTOR OF STANDARDIZED RESIDUALS
32      DO 30 I=1,N
33      IF (X(I).LE.0.0) GO TO 30
34      RES(I)=RES(I)/X(I)
35      CONTINUE
36      C----- GENERATE PLOT OF STANDARDIZED RESIDUALS VS. INDEPENDENT VARIABLE
37      CALL PLOTC (RES, HOR, CHAR, NK, 2)
38      RETURN
39

```

```

CPR*MS(1).PPREP(2) SUBROUTINE PPREP ( T, BCOEF, SCRATCH, BREAK, COEF, KX, JX, NB, MO, IP)
1
2
3      C----- PPREP  WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
4      C----- DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
5      C----- AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
6      C----- FOR: CONVERTING THE B-REPRESENTATION OF THE SPLINE INTO THE
7      C----- PIECEWISE POLYNOMIAL REPRESENTATION
8      C----- SUBPROGRAMS CALLED: BSPLPP
9      C----- CURRENT VERSION COMPLETED APRIL 3, 1980
10
11      DIMENSION T(KX),BCOEF(KX),SCRATCH(JX,JX),BREAK(KX),COEF(JX,KX),
12      C----- 2 11(20)          PPREP001
13      C----- 2 11H*          PPREP002
14      10     FORMAT (//1X,50(1H-)/1X,38H* PIECEWISE POLYNOMIAL REPRESENTATION , PPREP013
15      11     2 12HOF SPLINES *1X,50(1H-)//9X,18H. . . INTERVAL. . . '9X,          PPREP014
16      12     3 27HCOEFFICIENTS OF (X-X(1))**P//3X,1H,6X,4H(X(1),7X,6H(X(I+1),5X,          PPREP015
17      13     4 3HP =,8(14,8X)/35X,8(14,8X)/35X,4(14,8X)          PPREP016
18      20     FORMAT (1X,13,2X,2G12.5,3X,8G12.5/33X,8G12.5/33X,4G12.5)          PPREP017
19      30     FORMAT ()          PPREP018
20      40     FORMAT (//1X,42H***** PRINTOUT OF PIECEWISE POLYNOMIALS ,          PPREP019
21      2 18HSUPPRESSED *****)          PPREP020
22      C--- COMPUTE PIECEWISE POLYNOMIAL REPRESENTATION OF SPLINE          PPREP021
23      C--- CALL BSPLPP (T, BCOEF, NB, MO, SCRATCH, BREAK, COEF, L, JX)          PPREP022
24      C--- DIVIDE EACH COEF(J,1) BY (J-1) FACTORIAL TO NORMALIZE          PPREP023
25      IF (MO.LT.3) GO TO 80          PPREP024
26      DO 70 I=1,L          PPREP025
27      DO 60 J=3,MO          PPREP026
28      DO 50 K=3,J          PPREP027
29      COEF(J,1)=COEF(J,1)/FLOAT(K-1)          PPREP028
30      CONTINUE          PPREP029
31      50      CONTINUE          PPREP030
32      60      CONTINUE          PPREP031
33      70      CONTINUE          PPREP032
34      80      IF ( IP .EQ. 0) GO TO 110          PPREP033
35      DO 90 I=1,MO          PPREP034
36      90      I(I,I)=I-1          PPREP035
37      CONTINUE          PPREP036
38      WRITE (6,10) (I(I,I),I=1,MO)          PPREP037
39      WRITE (6,30)          PPREP038
40      DO 100 I=1,L          PPREP039
41      100      WRITE (6,20) I,BREAK(I), (COEF(J,I),J=1,MO)          PPREP040
42      CONTINUE          PPREP041
43      RETURN          PPREP042
44      WRITE (6,40)          PPREP043
45      RETURN          PPREP044

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1  CPPR*NS(1) .RESSD(1)  SUBROUTINE RESSD (X, Y, W, N, NX, NKK, NRS, T, BCOEF, XXI, K, KK, NB, MO, YHAT, RESSD001
2  RES, RSD, BIATX, JX, IP)  RESSD002
3  C-----  RESSD003
4  C-----  WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING  RESSD004
5  C-----  DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.  RESSD005
6  C-----  AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION  RESSD006
7  C-----  FOR: COMPUTING PREDICTED Y-VALUES, STANDARD DEVIATIONS OF  RESSD007
8  C-----  PREDICTED Y-VALUES, AND THE RESIDUAL STANDARD DEVIATION  RESSD008
9  C-----  SUBPROGRAMS CALLED: BVALUE, INTERV, BSPLVB  RESSD009
10 C-----  CURRENT VERSION COMPLETED MARCH 24, 1980  RESSD010
11 C-----  RESSD011
12  DIMENSION X(NX),Y(NX),W(NX),T(NX),BCOEF(KX),YHAT(NKK),RES(NKK),  RESSD012
13  2 BIATX(JX),XXI(KX,KX)  RESSD013
14  10 FORMAT (//1X,25(1H-)/1X,25H* ANALYSIS OF RESIDUALS */1X,25(1H-)//  RESSD014
15  15 2 9X,6HWEIGHT,20X,8HOBERVED,5X,9HPREDICTED,20X,10HSTD DEV OF/4X,  RESSD015
16  16 3 1H1,5X,4HW(1),9X,4HW(1),10X,4HY(1),10X,4HY(1),6X,11HRESIDUAL(1).  RESSD016
17  17 4 3X,14HPREDICTED Y(1) )  RESSD017
18  20 FORMAT (1X,I4,2X,G11.5,3G14.7,G12.5,G16.7)  RESSD018
19  30 FORMAT (//5X,16HRESIDUAL STD DEV,5X,13HRESIDUAL D.F./7X,G12.6,9X,  RESSD019
20  2 15)  RESSD020
21  40 FORMAT (/1X,4BH***** PRINTOUT OF RESIDUALS SUPPRESSED *****)  RESSD021
22  C---  INITIALIZE SUMMING VARIABLE  RESSD022
23  SUM=0.0  RESSD023
24  IF (IP.EQ.0) WRITE (6,40)  RESSD024
25  IF (IP.NE.0) WRITE (6,10)  RESSD025
26  C---  COMPUTE PREDICTED VALUES AND RESIDUALS  RESSD026
27  DO 50 I=1,N  RESSD027
28  XX=X(I)  RESSD028
29  YHAT(I)=BVALUE(T,BCOEF,NB,MO,XX,0)  RESSD029
30  RES(I)=Y(I)-YHAT(I)  RESSD030
31  SUM=SUM+W(I)*RES(I)**2  RESSD031
32  CONTINUE  RESSD032
33  C---  COMPUTE RESIDUAL STANDARD DEVIATION  RESSD033
34  RSD=SQRT(SUM/FLOAT(NRS))  RESSD034
35  C---  COMPUTE STANDARD DEVIATIONS OF PREDICTED VALUES  RESSD035
36  DO 90 L=1,N  RESSD036
37  XX=X(L)  RESSD037
38  C---  FIND INDEX OF FIRST KNOT TO LEFT OF X-VALUE  RESSD038
39  39 CALL INTERV (T,K,XX,LEFT,MFLAG)  RESSD039
40  C---  CHECK WHETHER X-VALUE LIE WITHIN KNOT SPAN  RESSD040
41  IF (MFLAG.EQ.0) GO TO 60  RESSD041
42  C---  SET RESIDUAL TO ZERO FOR X-VALUE OUTSIDE KNOT SPAN  RESSD042
43  RES(L)=0.0  RESSD043
44  C---  SET STANDARD DEVIATION OF RESIDUAL TO ZERO  RESSD044
45  YHAT(L)=0.0  RESSD045
46  GO TO 90  RESSD046
47  C---  EVALUATE POSSIBLY NON-ZERO B-SPLINES AT X-VALUE  RESSD047
48  60 CALL BSPLVB (T,MO,1,XX,LEFT,BIATX)  RESSD048
49  C---  COMPUTE VARIANCE COEFFICIENT (BIATX)' (XXI) (BIATX) OF  RESSD049
50  C---  PREDICTED Y-VALUE  RESSD050
51  NLOW=LEFT-MO  RESSD051
52  Q1=0.0  RESSD052
53  DO 80 I=1,MO  RESSD053
54  Q2=0.0  RESSD054
55  N1=NLOW+I  RESSD055
56  DO 70 J=1,MO  RESSD056
57  NJ=NLOW+J  RESSD057

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58      Q2=Q2+BIATX(J)*XXXI(NJ,NI)
59      CONTINUE
60      Q1=Q1+Q2*BIATX(1)
61      CONTINUE
62      C--- COMPUTE STANDARD DEVIATION OF PREDICTED Y-VALUE
63      YHATSD=RSD*SQRT(Q1)
64      IF (1P.EQ.0) GO TO 90
65      WRITE (6,20) L,W(L),X(L),Y(L),YHAT(L),RES(L),YHATSD
66      C--- COMPUTE STANDARD DEVIATION OF EACH RESIDUAL AND STORE IN
67      C--- VECTOR *YHAT*
68      YHAT(L)=SQRT(RSD**2-YHATSD**2)
69      CONTINUE
70      WRITE (6,30) RSD,NRSD
71      RETURN
72      END

```

CPR*RSQ(1) .RSQ(3) SUBROUTINE RSQ (RSD, NRS, Y, W, N, NX, NWZ)

```

1      RSQ*RSQ( 1 ) .RSQ( 3 ) SUBROUTINE RSQ ( RSD, NRS, Y, W, N, NX, NWZ )
2
3      C----- RSQ  WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
4      C----- DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
5      C----- AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
6      C----- FOR: COMPUTING THE MULTIPLE CORRELATION COEFFICIENT R-SQUARE
7      C----- SUBPROGRAMS CALLED: -NONE-
8      C----- CURRENT VERSION COMPLETED JUNE 11, 1980
9
10     C----- DIMENSION Y(NX), W(NX)
11     C----- 10  FORMAT ( //7X, BHR SQUARE, 7X, 26HNUMBER OF NON-ZERO WEIGHTS/4X, F11.8, RSQ00011
12     C----- 2 16X, 15)
13     C----- COMPUTE RESIDUAL SUM OF SQUARES
14     C----- RSS=FLOAT( NRS ) * RSD**2
15     C----- INITIALIZE SUMMING VARIABLE
16     C----- TSS=0.0
17     DO 20  I=1, N
18     TSS=TSS+Y( I ) * SQRT( W( I ) )
19     CONTINUE
20     YM=TSS/FLOAT( NZ )
21     C----- INITIALIZE SUMMING VARIABLE
22     C----- TSS=0.0
23     C----- COMPUTE TOTAL SUM OF SQUARES
24     DO 30  I=1, N
25     IF ( W( I ) .EQ. 0.0 ) GO TO 30
26     TSS=TSS+( Y( I ) * SQRT( W( I ) ) - YM ) **2
27     CONTINUE
28     C----- COMPUTE R**2
29     C----- R2= 1.0 - RSS/TSS
30     C----- TO PRINT OUT R-SQUARED CHANGE THE 'C' IN THE FOLLOWING LINE
31     C----- TO A BLANK.
32     C----- WRITE ( 6, 10 ) R2, NZ
33     RETURN
34

```

```

RSQ00001
RSQ00002
RSQ00003
RSQ00004
RSQ00005
RSQ00006
RSQ00007
RSQ00008
RSQ00009
RSQ00010
RSQ00011
RSQ00012
RSQ00013
RSQ00014
RSQ00015
RSQ00016
RSQ00017
RSQ00018
RSQ00019
RSQ00020
RSQ00021
RSQ00022
RSQ00023
RSQ00024
RSQ00025
RSQ00026
RSQ00027
RSQ00028
RSQ00029
RSQ00030
RSQ00031
RSQ00032
RSQ00033
RSQ00034

```


CPR*NS(1) . SORT1(2) SymposiN SOBT1 (X N N N)

```

58      80      KN=L.Q(1)
59      81      IF (KN-KM.GE. 11) GO TO 10
60      82      KM=KM-1
61      83      KM=KM+1
62      84      IF (KM.EQ.KN) GO TO 70
63      85      A=X(KM+1)
64      86      IF (X(KM).LE.A) GO TO 90
65      87      J=KM
66      88      X(J+1)=X(J)
67      89      J=J-1
68      90      IF (J.EQ.M-1) GO TO 110
69      91      IF (A.LT.X(J)) GO TO 100
70      92      X(J+1)=A
71      93      GO TO 90
72      94      END

```

SORT1058
 SORT1059
 SORT1060
 SORT1061
 SORT1062
 SORT1063
 SORT1064
 SORT1065
 SORT1066
 SORT1067
 SORT1068
 SORT1069
 SORT1070
 SORT1071
 SORT1072

CPRTNS(1) . SORT2(3) SUBROUTINE SORT2 (X, Y, M, N, NX)

```

1      C-----SUBROUTINE SORT2 (X, Y, M, N, NX)
2      C
3      C      OBTAINED BY CHARLES P. REEVE FROM DR. D. A. ZAHN AT
4      C      THE FLORIDA STATE UNIVERSITY, TALLAHASSEE, FLORIDA
5      C      UNDER THE NAME *FTASORT*.  SEVERAL MINOR CORRECTIONS
6      C      WERE MADE TO THE ORIGINAL VERSION AFTER LINE 61.
7      C      THE PROGRAM HAS BEEN ALTERED SO THAT A SECOND ARRAY IS
8      C      CARRIED ALONG AND SORTED IDENTICALLY AS THE FIRST
9      C      FOR: SORTING THE SEGMENT OF A REAL ARRAY BETWEEN ENTRIES
10     C      M AND N FROM SMALLEST TO LARGEST
11     C      SUBROUTINES CALLED: -NONE-
12     C      CURRENT VERSION COMPLETED MARCH 24, 1980
13     C      NOTE: ARRAYS LP(K) AND LQ(K) PERMIT SORTING UP TO 2***(K+1)-1
14     C      ELEMENTS.  I.E., FOR K=25 YOU MAY SORT 67,108,863 ELEMENTS.
15
16     DIMENSION LP(25), LQ(25), X(NX), Y(NX)
17     I=1
18     KN=M
19     KN=N
20     IF (KM.GE.KN) GO TO 70
21     J=KM
22     K=(KN+KD)/2
23     A=X(K)
24     B=Y(K)
25     IF (X(KD).LE.A) GO TO 20
26     X(KD)=X(KD)
27     Y(KD)=Y(KD)
28     X(KD)=A
29     Y(KD)=B
30     A=X(K)
31     B=Y(K)
32     L=KN
33     IF (X(KN).GE.A) GO TO 40
34     X(KD)=X(KN)
35     Y(KD)=Y(KN)
36     X(KN)=A
37     Y(KN)=B
38     A=X(K)
39     B=Y(K)
40     IF (X(KD).LE.A) GO TO 40
41     X(KD)=X(KD)
42     Y(KD)=Y(KD)
43     X(KD)=A
44     Y(KD)=B
45     A=X(K)
46     B=Y(K)
47     GO TO 40
48     X(L)=X(J)
49     Y(L)=Y(J)
50     X(J)=G
51     Y(J)=H
52     L=L-1
53     IF (X(L).GT.A) GO TO 40
54     G=X(L)
55     H=Y(L)
56     J=J+1
57     IF (X(J).LT.A) GO TO 50

```

```

58 IF (J.LE.LJ) GO TO 30
59 IF (L-KM.LE.KN-J) GO TO 60
60 LP(I)=KM
61 LQ(I)=L
62 KM=J
63 I=I+1
64 GO TO 80
65 LP(I)=J
66 LQ(I)=KN
67 KN=L
68 I=I+1
69 GO TO 80
70 I=I-1
71 IF (I.EQ.0) RETURN
72 KM=LP(I)
73 KN=LQ(I)
74 IF (KN-KM.GE.1) GO TO 10
75 KM=KM-1
76 KM=KM+1
77 IF (KM.EQ.KN) GO TO 70
78 A=X(KM+1)
79 B=Y(KM+1)
80 IF (X(KM).LE.A) GO TO 90
81 J=KM
82 X(J+1)=X(J)
83 Y(J+1)=Y(J)
84 J=J-1
85 IF (J.EQ.M-1) GO TO 110
86 IF (A.LT.X(J)) GO TO 100
87 X(J+1)=A
88 Y(J+1)=B
89 GO TO 90
90 END

```

1 C SPLINE(N,1) . SPLINE(N,8) SUBROUTINE SPLEEN (H, X, Y, W, R1, R2, RES, N, NX, NXX, T, BCOEF, XX1, Q, DIAG, KSPLEE001
 2 C 2, KX, YY, NY, NYX, MD, SCRATCH, JX, AL, DL, C, IP)
 3 C SPLEEE002
 4 C SPLEEE003
 5 C SPLEEE004
 6 C SPLEEE005
 7 C SPLEEE006
 8 C SPLEEE007
 9 C SPLEEE008
 10 C SPLEEE009
 11 C SPLEEE010
 12 C SPLEEE011
 13 C SPLEEE012
 14 C SPLEEE013
 15 C SPLEEE014
 16 C SPLEEE015
 17 C SPLEEE016
 18 C SPLEEE017
 19 C SPLEEE018
 20 C SPLEEE019
 21 C SPLEEE020
 22 C SPLEEE021
 23 C SPLEEE022
 24 C SPLEEE023
 25 C SPLEEE024
 26 C SPLEEE025
 27 C SPLEEE026
 28 C SPLEEE027
 29 C SPLEEE028
 30 C SPLEEE029
 31 C SPLEEE030
 32 C SPLEEE031
 33 C SPLEEE032
 34 C SPLEEE033
 35 C SPLEEE034
 36 C SPLEEE035
 37 C SPLEEE036
 38 C SPLEEE037
 39 C SPLEEE038
 40 C SPLEEE039
 41 C SPLEEE040
 42 C SPLEEE041
 43 C SPLEEE042
 44 C SPLEEE043
 45 C SPLEEE044
 46 C SPLEEE045
 47 C SPLEEE046
 48 C SPLEEE047
 49 C SPLEEE048
 50 C SPLEEE049
 51 C SPLEEE050
 52 C SPLEEE051
 53 C SPLEEE052
 54 C SPLEEE053
 55 C SPLEEE054
 56 C SPLEEE055
 57 C SPLEEE056
 C
 C THIS PACKAGE OF SUBROUTINES WAS WRITTEN FOR THE FOLLOWING
 C CALIBRATION PROCEDURES:
 C
 C 1) A MONOTONIC SEQUENCE OF RESPONSES Y(1), Y(2), . . . , Y(N)
 C EACH CONTAINING SOME ERROR ARE OBSERVED AT KNOWN POINTS
 C X(1), X(2), . . . , X(N) WHERE X(1) < X(2) < . . . < X(N).
 C
 C 2) A SPLINE OF SPECIFIED DEGREE WITH A SPECIFIED SEQUENCE OF
 C FIXED KNOTS IS FIT TO THE Y-VALUES WHICH MAY BE WEIGHTED.
 C
 C 3) THE RESIDUAL STANDARD DEVIATION IS COMPUTED IN ORDER TO
 C MEASURE THE GOODNESS OF THE SPLINE FIT.
 C
 C 4) PREDICTED RESPONSE VALUES ARE COMPUTED AT A LARGE NUMBER
 C OF UNIFORMLY SPACED X-VALUES BETWEEN THE EXTREME KNOTS.
 C A CONFIDENCE INTERVAL FOR EACH PREDICTED RESPONSE IS
 C COMPUTED BASED ON SPECIFIED CONSTANTS ALPHA, BETA, AND C
 C IN ACCORDANCE WITH REFERENCE PAPER BY SCHEFFE GIVEN BELOW.
 C
 C 5) FOR SPECIFIED Y-VALUES, INVERSE INTERPOLATION IS APPLIED
 C TO THE CALIBRATION CURVE AND ITS CONFIDENCE BAND TO GIVE
 C PREDICTED X-VALUES WITH CORRESPONDING UPPER AND LOWER
 C CONFIDENCE LIMITS.
 C
 C PASSED PARAMETERS (AND DIMENSIONS):
 C
 C * H(80) = UP TO 80 CHARACTERS IN BOA1 FORMAT IDENTIFYING THE
 C DATA
 C
 C * X(NX) = VECTOR (LENGTH NX) OF X-VALUES WHERE OBSERVATIONS
 C WERE MADE (INDEPENDENT VARIABLE)
 C
 C * Y(NX) = VECTOR (LENGTH NX) OF OBSERVATIONS
 C
 C * W(NX) = VECTOR (LENGTH NX) OF WEIGHTS FOR OBSERVATIONS
 C
 C R1(NKX) = VECTOR (LENGTH NX+K) FOR SCRATCH AREA
 C R2(NKX) = VECTOR (LENGTH NX+K) FOR SCRATCH AREA
 C
 C RES(NKX) = VECTOR (LENGTH NX+K) OF RESIDUALS FROM SPLINE FIT
 C
 C * N = NUMBER OF OBSERVATIONS
 C
 C * NX = DIMENSION (>=N) OF VECTORS X, Y, W
 C
 C * NKX = DIMENSION (>=N+K) OF VECTORS R1, R2, RES

```

58 C * T(KX) = VECTOR ( LENGTH K+2*MD ) OF KNOT LOCATIONS
59 C
60 C BCOEF(KX) = VECTOR ( LENGTH K+MD-1 ) OF B-SPLINE COEFFICIENTS
61 C
62 C XXI(KX,KX) = VARIANCE-COVARIANCE MATRIX ( SIZE [ K+MD-1 ] X[ K+MD-1 ] )
63 C OF B-SPLINE COEFFICIENTS
64 C
65 C Q(JX,KX) = MATRIX ( SIZE [ MD+1 ] X[ K+MD-1 ] ) FOR SCRATCH AREA
66 C
67 C
68 C
69 C * K = NUMBER OF KNOTS SPECIFIED BY USER ( LATER INCREASED
70 C TO K+2*MD BY PROGRAM )
71 C
72 C * KX = DIMENSION ( >=K+2*MD ) OF VECTORS T, BCOEF ,DIAG AND
73 C MATRICES XXI AND Q ( COLUMN ONLY )
74 C
75 C * YY(NYX) = VECTOR ( LENGTH NY ) OF Y-VALUES FOR WHICH PREDICTED
76 C X-VALUES ( WITH CONFIDENCE INTERVALS ) ARE TO BE
77 C COMPUTED
78 C
79 C * NY = NUMBER OF Y-VALUES FOR WHICH PREDICTED X-VALUES
80 C ARE TO BE COMPUTED
81 C
82 C
83 C * NYX = DIMENSION ( >=NY ) OF VECTOR YY
84 C
85 C * MD = DEGREE OF SPLINE ( < =19 ) ; FOR EXAMPLE, 1=LINEAR,
86 C 2=QUADRATIC, 3=CUBIC
87 C
88 C SCRATCH(JX,JX) = MATRIX ( SIZE [ MD+1 ] X[ MD+1 ] ) FOR SCRATCH AREA
89 C
90 C * JX = DIMENSION OF SQUARE MATRIX SCRATCH AND ROW
91 C DIMENSION OF MATRIX Q = 26
92 C
93 C * AL = ALPHA LEVEL OF SIGNIFICANCE ( SEE REFERENCE BELOW )
94 C
95 C * DL = DELTA LEVEL OF SIGNIFICANCE ( SEE REFERENCE BELOW )
96 C
97 C * C = CONSTANT IN THE INTERVAL ( 0.85, 1.25 ) ASSOCIATED
98 C WITH SCHEFFE'S CALIBRATION TECHNIQUE
99 C
100 C * 0 FOR ABBREVIATED PRINTOUT ( NO RESIDUALS )
101 C * 1 FOR FULL PRINTOUT ( RESIDUALS, PP REPRESENTATION )
102 C * 2 FOR FULL PRINTOUT PLUS Y-CONFIDENCE INTERVALS FOR
103 C 300 EVENLY SPACED X-VALUES OVER KNOT SPAN
104 C
105 C * INDICATES THAT AN INPUT VALUE IS REQUIRED FOR THIS VARIABLE
106 C
107 C NOTE: THE USER IS NOT REQUIRED TO ORDER THE ELEMENTS OF ANY INPUT
108 C VECTOR. THE PROGRAM WILL AUTOMATICALLY ORDER THOSE VECTORS
109 C WHICH NEED TO BE ORDERED.
110 C
111 C REFERENCE: SCHEFFE, HENRY, 'A STATISTICAL THEORY OF CALIBRATION',
112 C THE ANNALS OF STATISTICS, VOLUME 1, NUMBER 1,
113 C JANUARY 1973, PP. 1-37
114 C
115 C SUBPROGRAMS CALLED: ADKNTS, CHECK1, CHECK2, CIYFIN, COVAR, L2APPR,

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116 PLOTSR, PPREP, RESSD, RSQ, SDYFIN, SORT1, SPLEE116
117 SORT2, XYFINE, YTOXCI SPLEE117
118 CURRENT VERSION COMPLETED JUNE 11, 1980 SPLEE118
119 SPLEE119
120 C--- SET DIMENSIONS OF VECTORS AND MATRIX SPLEE120
121 DIMENSION X(NX),Y(NX),W(NX),R1(NKX),R2(NKX),RES(NKX) SPLEE121
122 DIMENSION T(KX),Q(JX,KX),BOEF(KX),XX1(KX,KX) SPLEE122
123 DIMENSION YY(NYX),SCRATCH(JX,JX),BIATX(20),H(80) SPLEE123
124 PARAMETER NF=300 SPLEE124
125 DIMENSION XF(300),YF(300),YFU(300),YFSD(300) SPLEE125
126 FORMAT (1H1/1X,45(1H*)/1X,32H* FIXED-KNOT SPLINE PACKAGE FOR , SPLEE126
127 2 13HCALIBRATION */1X,45(1H*) ESTIMATION OF B- SPLINE , SPLEE127
128 2 FORMAT (//1X,39(1H-)/1X,25H*) SPLEE128
129 2 14HCOEFFICIENTS */1X,39(1H-) SPLEE129
130 39 FORMAT (//9X,8HB-B-SPLINE/4X,1H1,5X,4HCOEF,10X,7HSTD DEV/) SPLEE130
131 40 FORMAT (1X,14,2G15.8) SPLEE131
132 50 FORMAT (//1X,4.2H***** PRINTOUT OF B-SPLINE COEFFICIENTS , SPLEE132
133 2 18HSUPPRESSED ***** SPLEE133
134 60 FORMAT (//1X,42(1H-)/1X,37H* PARAMETERS OF LEAST SQUARES SPLINE , SPLEE134
135 2 5HFT */1X,42(1H-)/1X,18HDEGREE OF SPLINE = 14//3X, SPLEE135
136 3 28HNNUMBER OF OBSERVATIONS = 14//3X, SPLEE136
137 4 28HNNUMBER OF ZERO WEIGHTS = 14//3X, 19HNNUMBER OF NON-ZERO , SPLEE137
138 5 9HWEIGHTS = 14//3X, 28HNNUMBER OF KNOTS = 14//3X, SPLEE138
139 6 28HNNUMBER OF B-SPLINES = 14//11X, 18HNNUMBER OF Y-VALUES//7X SPLEE139
140 7,24HFOR WHICH X CONFIDENCE = 14//3X, 18HNINTERVAL IS TO BE , SPLEE140
141 8 BHCOMPUTED) SPLEE141
142 70 FORMAT (//5X,25H----- FULL PRINTOUT -----/) SPLEE142
143 80 FORMAT (//5X,32H----- ABBREVIATED PRINTOUT -----/) SPLEE143
144 90 FORMAT (//1X,80A1) SPLEE144
145 100 FORMAT (//1X,8(1H*)/1X,8H* STOP */1X,8(1H*)/) SPLEE145
146 C--- DEFINE NUMBER OF POINTS IN FINE MESH SPLEE146
147 NF=300 SPLEE147
148 C--- WRITE HEADING FOR HARDCOPY OUTPUT SPLEE148
149 148 WRITE (6,10) SPLEE149
150 C--- WRITE RUN IDENTIFICATION SPLEE150
151 150 WRITE (6,90) (H(I),I=1,80) SPLEE150
152 IF (IP.GE.1) WRITE (6,70) SPLEE151
153 IF (IP.EQ.0) WRITE (6,80) SPLEE152
154 C--- COMPUTE ORDER OF SPLINE SPLEE153
155 MO=MD+1 SPLEE154
156 C--- CHECK THAT INPUT PARAMETERS FALL WITHIN ALLOWABLE RANGES SPLEE155
157 SPLEE156
158 CALL CHECK1 (W,N,NX,K,KX,NKX,NY,NYX,JX,MO,AL,DL,C,NZ) SPLEE157
159 C--- SORT THE VECTOR OF KNOT LOCATIONS FROM LEAST TO GREATEST SPLEE158
160 C--- SPLEE159
161 C--- SPLEE160
162 C--- SPLEE161
163 C--- SPLEE162
164 C--- SPLEE163
165 C--- SPLEE164
166 C--- SPLEE165
167 C--- SPLEE166
168 C--- SPLEE167
169 C--- SPLEE168
170 C--- SPLEE169
171 C--- SPLEE170
172 C--- SPLEE171
173 C--- SPLEE172
174 C--- SPLEE173

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174      NZNZ=N-NZ
175      C--- DEFINE NEW VECTOR OF KNOTS WITH END POINTS DUPLICATED
176      C--- (MD) TIMES
177      C      CALL ADKNTS (T, KX, MO)
178      C--- COMPUTE NUMBER OF B-SPLINES
179      C      NB=K-MO
180      C--- COMPUTE NUMBER OF DEGREES OF FREEDOM FOR RESIDUALS
181      C      NRSD=NNZ-NB
182      C      NRSD=NNZ-NB
183      C      WRITE (6,60) MD,N,NZ,NNZ,K,NB,NY
184      C      WRITE (*,60) MD,N,NZ,NNZ,K,NB,NY
185      C--- COMPUTE ESTIMATES OF B-SPLINE COEFFICIENTS
186      C      CALL L2APPR (T,NB,MO,Q,DIAG,BCOEF,JX,K,N,X,Y,W)
187      C
188      C--- COMPUTE UNSCALED VARIANCE-COVARIANCE MATRIX OF
189      C--- B-SPLINE COEFFICIENTS
190      C
191      C      CALL COVAR (KX,NB,JX,MO,Q,XXI)
192      C
193      C--- COMPUTE (PREDICTED Y-VALUES AND) RESIDUAL STANDARD DEVIATION
194      C
195      C      CALL RESSD (X,Y,W,N,NX,NKX,NRSD,T,BCOEF,XXI,K,KX,NB,MO,R1,RES,RSD)
196      C      SPLEE196
197      C      SPLEE197
198      C
199      C      IF (IP.EQ.0) WRITE (6,50)
200      C      IF (IP.EQ.0) GO TO 120
201      C--- WRITE B-SPLINE COEFFICIENTS AND THEIR STANDARD DEVIATIONS
202      C      WRITE (6,20)
203      C      WRITE (6,30)
204      C      DO 110 I=1,NB
205      C      S=RSDF*SQRT(XXI(I,I))
206      C      WRITE (6,40) I,BCOEF(I),S
207      C
208      C--- COMPUTE MULTIPLE CORRELATION COEFFICIENT R-SQUARED ('THIS VALUE IS
209      C--- NOT PRINTED. TO PRINT R-SQUARED MAKE A CHANGE IN SUBROUTINE RSQ.')
210      C
211      C      110  CONTINUE
212      C
213      C--- CREATE FINE MESH OF EVENLY SPACED X-VALUES BETWEEN END KNOTS
214      C--- AND COMPUTE PREDICTED Y-VALUES THERE
215      C
216      C      CALL XYFLINE (NF,T,BCOEF,K,KX,NB,MO,XF,YF)
217      C
218      C--- COMPUTE STANDARD DEVIATION OF PREDICTED Y-VALUES
219      C      CALL SDYFIN (XF,YFSD,NF,T,K,MO,XXI,KX,RSD,BIATX,JX)
220      C
221      C--- COMPUTE CONFIDENCE INTERVALS FOR PREDICTED Y-VALUES USING
222      C--- SCHEFFE'S TECHNIQUE (SEE REFERENCE IN SUBROUTINE CIYFIN)
223      C
224      C      CALL CIYFIN (XF,YF,YFSD,NF,RSD,AL,DL,C,NRSD,NB,YFL,YFU,IP)
225      C
226      C--- COMPUTE X CONFIDENCE INTERVALS FOR SPECIFIED Y-VALUES
227      C
228      C      CALL YTOXCI (XF,YFL,YF,YFU,NF,YY,NY,NYX)
229      C
230      C--- COMPUTE PIECEWISE POLYNOMIAL REPRESENTATION OF SPLINE
231      C

```

232 C SPLEEF232
233 C SPLEEF233
234 C SPLEEF234
235 C SPLEEF235
236 C SPLEEF236
237 C SPLEEF237
238 C SPLEEF238
239 C SPLEEF239
240 C SPLEEF240
241 C SPLEEF241

C CALL PPREP (T, BCOEF, SCRTCH, DIAG, Q, KX, JX, NB, MO, IP)
C--- PLOT KNOT LOCATIONS AND RESIDUALS VS. INDEPENDENT VARIABLE
C CALL PLOTSR (X, N, NX, R1, RES, R2, NKK, T, K, KX)
C WRITE (6, 100)
C RETURN
C END

```

1  CPR*NS(1).XYFINE(1) SUBROUTINE XYFINE (NF, T, BCOEF, K, XX, NB, MO, XF, YF)
2  C
3  C      XYFINE      WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
4  C      DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
5  C      AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
6  C      FOR: CREATING A FINE MESH OF VALUES OVER THE DOMAIN OF X-VALUES
7  C      WHERE OBSERVATIONS WERE MADE AND COMPUTING CORRESPONDING
8  C      PREDICTED Y-VALUES
9  C      SUBPROGRAMS CALLED: BVALUE
10 C      CURRENT VERSION COMPLETED MARCH 19, 1980
11 C
12 C      DIMENSION T(KX), BCOEF(KX), XF(NF), YF(NF)
13 C      --- CREATE FINE MESH OF X VALUES OVER INTERVAL SPANNED BY KNOTS
14 C      FORMAT ('/5X,13H<<< GRID OF,15,1X,24H EVENLY SPACED X VALUES ,'
15 C      2 13HCREATED >>>)
16 C      C= (T(K)-T(1))/FLOAT(NF-1)
17 DO 20 I=1,NF
18 XF(1)=FLOAT(I-1)*C+T(1)
19 20 CONTINUE
20 C      --- COMPUTE PREDICTED Y VALUE AT EACH X VALUE
21 DO 30 I=1,NF
22 XX=XF(I)
23 YF(I)=BVALUE(T, BCOEF, NB, MO, XX, 0)
24 30 CONTINUE
25 WRITE (6,10) NF
26 RETURN
27 END

```

CPRNS(1). YTOXC1(8) SUBROUTINE YTOXC1 (XF, YFL, YF, YFU, NF, YY, NY, NYX)

```

1      YTOXC001
2      C----- SUBROUTINE YTOXC1 (XF, YFL, YF, YFU, NF, YY, NY, NYX)
3      C----- WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
4      C----- DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D. C.
5      C----- AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
6      C----- FOR: COMPUTING X CONFIDENCE INTERVALS FOR GIVEN Y-VALUES BY
7      C----- INVERSE INTERPOLATION ON THE CALIBRATION CURVE AND ITS
8      C----- UPPER AND LOWER BOUNDS
9      C----- SUBPROGRAMS CALLED: GETX, SORT1
10     C----- CURRENT VERSION COMPLETED SEPTEMBER 3, 1980
11
12     DIMENSION XF(NF), YFL(NF), YF(NF), YFU(NF), YY(NYX), IND(6)
13     DATA IND(1), IND(2), IND(3), IND(4), IND(5), IND(6) /1H, 1HS, 1HL, 1H*, 
14           2 1H<, 1H</
15     FORMAT (/*5X,40H<<< NO Y-VALUES SPECIFIED FOR INVERSE , 
16           2 19HINTERPOLATION >>>)
17     FORMAT (/*1X,47H*** LOWER CONFIDENCE CURVE IS NOT MONOTONIC AT , 
18           2 4HYFL( 14,3H) = ,G12.7/5X,21HNO INTERPOLATION DONE)
19     FORMAT (/*1X,45H*** CALIBRATION CURVE IS NOT MONOTONIC AT YF( , I4, 
20           2 3H) = ,G12.7/5X,21HNO INTERPOLATION DONE)
21     FORMAT (/*1X,47H*** UPPER CONFIDENCE CURVE IS NOT MONOTONIC AT , 
22           2 4HYFU( 14,3H) = ,G12.7/5X,21HNO INTERPOLATION DONE)
23     FORMAT (/*1X,65( 1H-)/1X,29H* COMPUTATION OF CALIBRATION , 
24           2 36HINTERVALS BY INVERSE INTERPOLATION */1X,65( 1H-)/24X, 
25           3 1HLOWER LIMIT,7X,9HPREDICTED,7X,1HUPPER LIMIT/4X,1HI,6X,4HY( I) , 
26           4 12X,5HFOR X,14X,1HX,14X,5HFOR X)
27     FORMAT (1X, 14, G15.7, 3(3X,A1,G13.7))
28     FORMAT (/*1X,46H*** AT LEAST ONE Y-VALUE IS OUTSIDE THE RANGE , 
29           2 3H***/1X,49H*** OF AT LEAST ONE CALIBRATION CURVE ****/)
30     FORMAT (/*5X,40HS DENOTES THE VALUE OF THE SMALLEST KNOT)
31     FORMAT (/*5X,40HL DENOTES THE VALUE OF THE LARGEST KNOT)
32     FORMAT (/*5X,41H* DENOTES VALUES OUTSIDE THE RANGE OF THE, 
33           2 22H CALIBRATION DATA - NO/7X,29HVAL ID PREDICTION IS AVAILABLE)
34     FORMAT (/*5X,49H< INDICATES THAT NO VALID LOWER CALIBRATION LIMIT< 
35           2 7X,55HGREATER THAN THE MINIMUM POSSIBLE X-VALUE IS AVAILABLE.)
36     FORMAT (/*5X,49H< INDICATES THAT NO VALID UPPER CALIBRATION LIMIT< 
37           2 7X,55HSMALLER THAN THE MAXIMUM POSSIBLE X-VALUE IS AVAILABLE.)
38     WRITE (6,50)
39     IF (NY.LT. 1) GO TO 230
40     M=1
41     IF (YF(1).GT. YF(NF)) M=-1
42     NF1=NF-1
43     C---- CHECK WHETHER CALIBRATION CURVE AND BOUNDS ARE MONOTONIC
44     DO 150 J=1, NF1
45     D=(YFL(J+1)-YFL(J))*FLOAT(M)
46     IF (D.GT.0.0) GO TO 130
47     J1=J+1
48     WRITE (6,20) J1, YFL(J1)
49     RETURN
50     D=(YF(J+1)-YF(J))*FLOAT(M)
51     IF (D.GT.0.0) GO TO 140
52     J1=J+1
53     WRITE (6,30) J1, YF(J1)
54     RETURN
55     D=(YFU(J+1)-YFU(J))*FLOAT(M)
56     IF (D.GT.0.0) GO TO 150
57     J1=J+1

```

```

58      WRITE ( 6,40) J1, YFU( J1)
59      RETURN
60      150  CONTINUE
61      C--- ORDER VECTOR OF Y-VALUES FOR WHICH X CONFIDENCE LIMITS ARE TO
62      C--- BE COMPUTED
63      CALL SORT1 ( YY, 1, NY, NYX )
64      L1=0
65      L2=0
66      L3=0
67      KS=0
68      KL=0
69      C--- IF CURVE IS MONOTONE DECREASING INVERT VECTORS ASSOCIATED
70      C--- WITH FINE MESH OF POINTS
71      IF ( M, EQ, 1) GO TO 170
72      NHALF=NF/2
73      DO 160 I=1, NHALF
74      J=NF+1-I
75      Q=XF(1)
76      XF(1)=XF( J)
77      XF( J)=Q
78      Q=YFL(1)
79      YFL(1)=YFL( J)
80      YFL( J)=Q
81      Q=YF(1)
82      YF(1)=YF( J)
83      YF( J)=Q
84      Q=YFU(1)
85      YFU(1)=YFU( J)
86      YFU( J)=Q
87      CONTINUE
88      DO 220 J=1, NY
89      Y=YY(J)
90      C--- GET THREE (3) X-VALUES BY INVERSE INTERPOLATION
91      CALL GETX (XF, YFL, NF, Y, L1, M, XU, I3, KS, KL)
92      IF ( I3, EQ, 1) GO TO 180
93      I3=(3-15*M4+2*I3+6*M*I3)/2
94      CALL GETX (XF, YF, NF, Y, L2, M, X, I2, KS, KL)
95      IF ( I2, EQ, 1) GO TO 190
96      I2=4
97      X=0.
98      CALL GETX (XF, YFU, NF, Y, L3, M, XL, I1, KS, KL)
99      IF ( I1, EQ, 1) GO TO 200
100     I1=(3+15*M4+2*I1-6*M*I1)/2
101     C--- IF CURVE IS MONOTONE DECREASING REVERSE LIMITS
102     IF ( M, EQ, 1) GO TO 210
103     D=XL
104     XL=XU
105     XU=D
106     I=11
107     I1=13
108     I3= I
109     210  WRITE ( 6,60) J, Y, IND( 11), XL, IND( 12), X, IND( 13), XU
110     220  CONTINUE
111     C--- FLAG Y-VALUES WHICH GIVE INTERPOLATED X-VALUES OUTSIDE THE KNOT
112     C--- SPAN
113     IF ( KS+KL, EQ, 0) RETURN
114     WRITE ( 6,70)
115     WRITE ( 6,80)

```

```
116      WRITE ( 6, 90)
117      WRITE ( 6, 100)
118      WRITE ( 6, 110)
119      WRITE ( 6, 120)
120      RETURN
121      WRITE ( 6, 10)
122      RETURN
123      END
230
```

```
YTOXC116
YTOXC117
YTOXC118
YTOXC119
YTOXC120
YTOXC121
YTOXC122
YTOXC123
```

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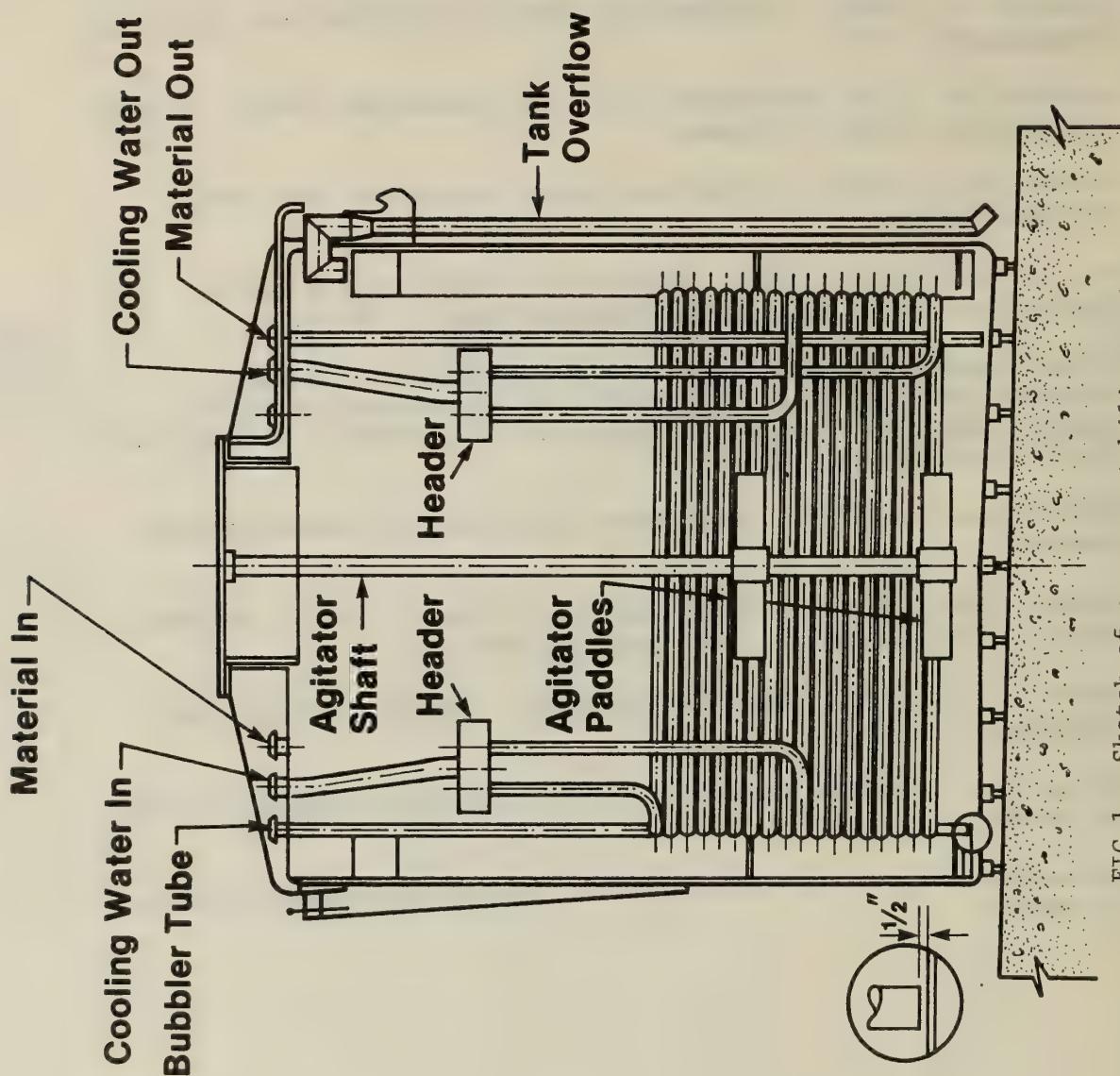


FIG. 1. Sketch of an accountability tank.

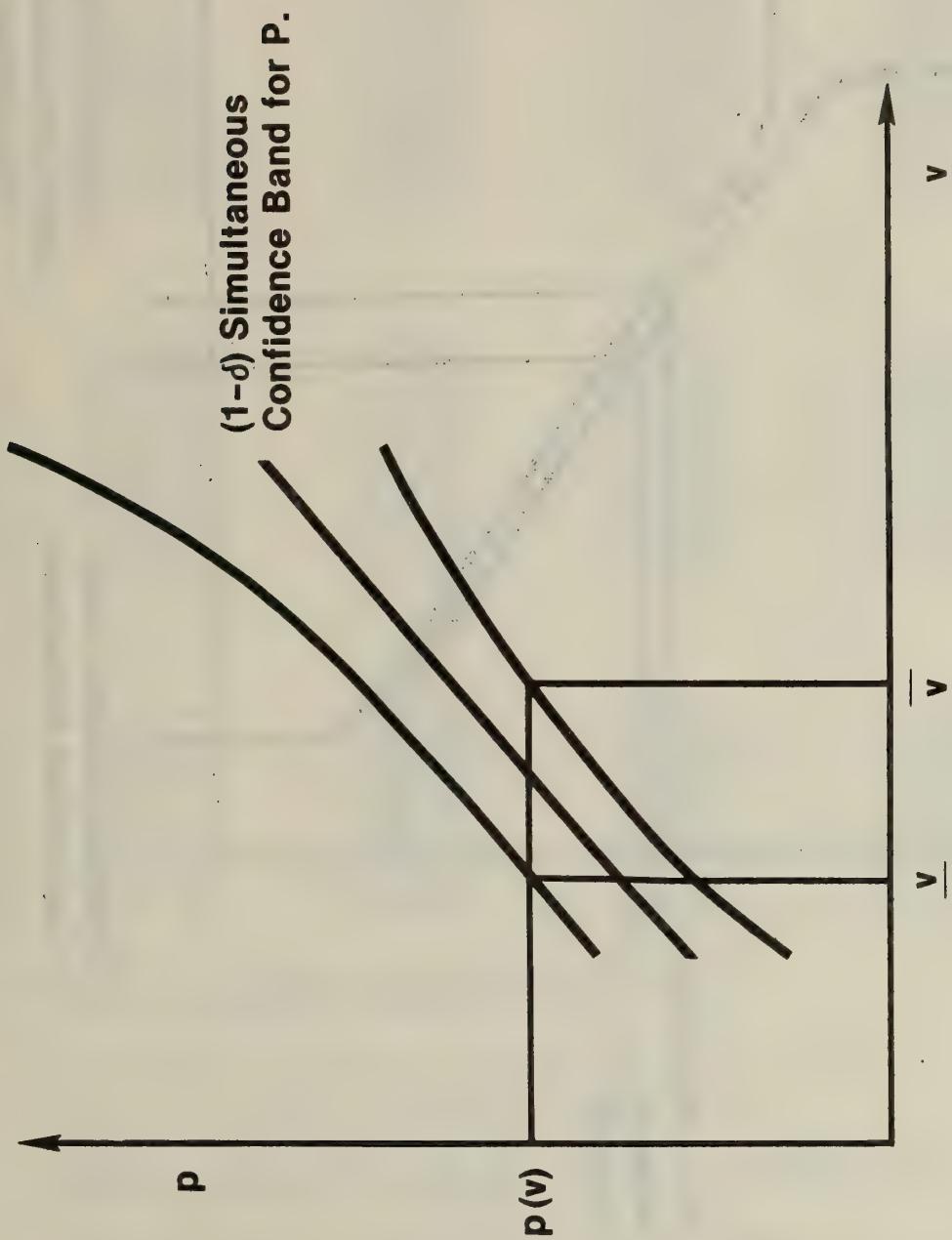


FIG. 2. Hypothetical Interval for v obtained from an exact value of $p = p(v)$.

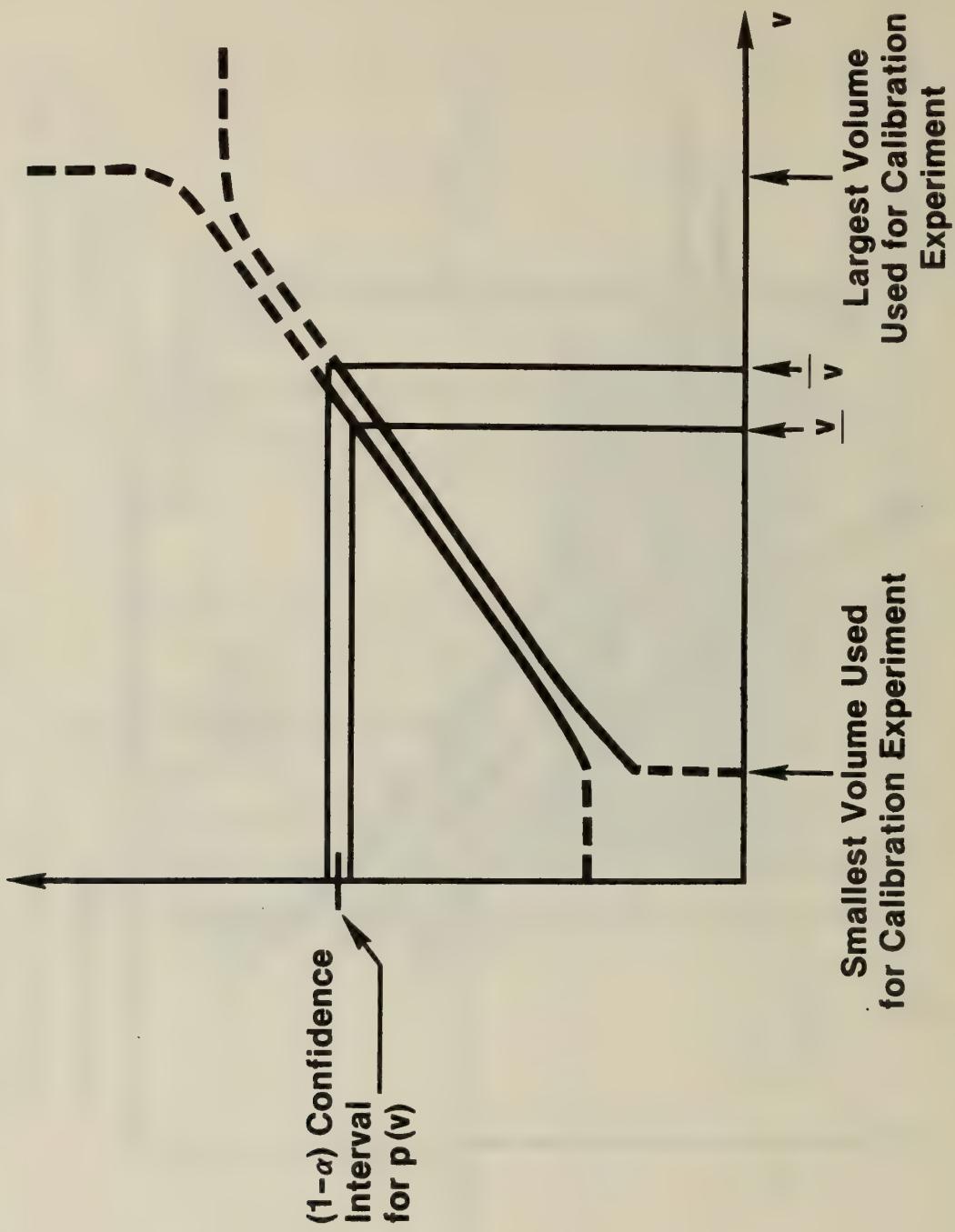


FIG. 3. Schematic for approximate construction of the calibration intervals.

* COMPUTATION OF CALIBRATION INTERVALS BY INVERSE INTERPOLATION *

I	Y(I)	LOWER LIMIT FOR X	PREDICTED X	UPPER LIMIT FOR X
1	3713.000	< 1.705250	1.705890	1.709779
2	3823.000	1.749691	1.753002	1.756223
3	3933.000	1.797422	1.800113	1.802745
4	4043.000	1.844952	1.847225	1.849473
5	4153.000	1.892090	1.894297	1.896511
6	4263.000	1.939002	1.941202	1.943401
7	4373.000	1.985893	1.988067	1.990239
8	4483.000	2.032783	2.034931	2.037077
9	4593.000	2.079673	2.081796	2.083916
10	4703.000	2.126563	2.128660	2.130755
11	4813.000	2.173453	2.175560	2.177668
12	4923.000	2.220343	2.222450	2.224558
13	5033.000	2.267233	2.269340	2.271448
14	5143.000	2.314123	2.316230	2.318338
15	5253.000	2.360913	2.363020	2.365128
16	5363.000	2.407803	2.409910	2.411998
17	5473.000	2.454693	2.456800	2.458908
18	5583.000	2.501583	2.503690	2.505798
19	5693.000	2.548473	2.550580	2.552688
20	5803.000	2.595363	2.597470	2.599578
21	5913.000	2.642253	2.644360	2.646468
22	6023.000	2.689143	2.691250	2.693358
23	6133.000	2.735933	2.738040	2.740148
24	6243.000	2.782823	2.784930	2.787038
25	6353.000	2.829713	2.831820	2.833928
26	6463.000	2.876603	2.878710	2.880818
27	6573.000	2.923493	2.925600	2.927708
28	6683.000	2.970383	2.972490	2.974598
29	6793.000	3.017273	3.019380	3.021488
30	6903.000	3.064163	3.066270	3.068378
31	7013.000	3.110953	3.113060	3.115168
32	7123.000	3.157843	3.160950	3.163058
33	7233.000	3.204733	3.206840	3.208948
34	7343.000	3.251623	3.253730	3.255838
35	7453.000	3.298513	3.300620	3.302728
36	7563.000	3.345403	3.347510	3.349618
37	7673.000	3.392293	3.394400	3.396508
38	7783.000	3.439183	3.441290	3.443398
39	7893.000	3.486073	3.488180	3.490288
40	8003.000	3.532963	3.535070	3.537178
41	8113.000	L 13.64334	* .0000000	> 13.64334
42	8223.000	L 13.64334	* .0000000	> 13.64334

*** AT LEAST ONE Y-VALUE IS OUTSIDE THE RANGE ***
 *** OF AT LEAST ONE CALIBRATION CURVE ***

S DENOTES THE VALUE OF THE SMALLEST KNOT

L DENOTES THE VALUE OF THE LARGEST KNOT

* DENOTES VALUES OUTSIDE THE RANGE OF THE CALIBRATION DATA - NO VALID PREDICTION IS AVAILABLE

< INDICATES THAT NO VALID LOWER CALIBRATION LIMIT GREATER THAN THE MINIMUM POSSIBLE X-VALUE IS AVAILABLE.

> INDICATES THAT NO VALID UPPER CALIBRATION LIMIT SMALLER THAN THE MAXIMUM POSSIBLE X-VALUE IS AVAILABLE.

Figure 4. Calibration chart. Y is pressure in pascals; X is volume in M^3 .

* FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION *

REAL DATA FROM A TANK CALIBRATION (DATA IN FILE CPR*NS.96)

----- FULL PRINTOUT -----

<<<< EACH END KNOT DUPLICATED 1 TIMES >>>>

* SUMMARY OF KNOT LOCATIONS *

I	KNOTS(I)
1	1.70525
2	1.70525
3	1.89466
4	4.54674
5	5.49482
6	5.87381
7	6.44156
8	7.18990
9	10.0425
10	10.2320
11	12.5044
12	13.6433
13	13.6433

* PARAMETERS OF LEAST SQUARES SPLINE FIT *

DEGREE OF SPLINE = 1

NUMBER OF OBSERVATIONS = 172
NUMBER OF ZERO WEIGHTS = 0
NUMBER OF NON-ZERO WEIGHTS = 172
NUMBER OF KNOTS = 13
NUMBER OF B-SPLINES = 11

NUMBER OF Y VALUES
FOR WHICH X CONFIDENCE = 242
INTERVAL IS TO BE COMPUTED

<<<< 11 B-SPLINE COEFFICIENTS COMPUTED >>>>

Figure 5. Preliminaries.

* ANALYSIS OF RESIDUALS *

I	WEIGHT W(I)	X(I)	OBSERVED Y(I)	PREDICTED Y(I)	RESIDUAL(I) Y(I)	STD DEV OF PREDICTED Y(I)
1	1.0000	1.705250	3711.640	3711.505	.13455	1.052565
2	1.0000	1.705270	3711.420	3711.552	-.13223	1.052453
3	1.0000	1.894010	4152.240	4152.238	.18311-02	.4110981
4	1.0000	1.894140	4152.130	4152.542	-.41168	.4113765
5	1.0000	1.894580	4151.050	4153.569	-2.5190	.4123280
6	1.0000	1.894650	4151.910	4153.732	-1.8225	.4124807
7	1.0000	1.894660	4153.400	4153.756	-.35577	.4125026
8	1.0000	2.084060	4599.320	4598.315	1.0054	.3729185
9	1.0000	2.084110	4600.090	4598.432	1.6581	.3729083
10	1.0000	2.272720	5044.100	5041.136	2.9636	.3359134
11	1.0000	2.273020	5042.730	5041.841	.88947	.3358569
162	1.0000	13.07486	28884.68	28883.46	1.2214	.2921614
163	1.0000	13.26022	29282.92	29282.06	.86230	.3425575
164	1.0000	13.26158	29285.71	29284.98	.72754	.3430482
165	1.0000	13.26232	29284.50	29286.57	-2.0735	.3433159
166	1.0000	13.45198	29695.29	29694.42	.87061	.4235761
167	1.0000	13.45385	29699.14	29698.44	.69897	.4244610
168	1.0000	13.63914	30096.50	30096.89	-.38940	.5180907
169	1.0000	13.64052	30099.62	30099.86	-.23706	.5188241
170	1.0000	13.64133	30098.26	30101.60	-3.3391	.5192548
171	1.0000	13.64143	30102.36	30101.81	.54614	.5193080
172	1.0000	13.64333	30105.91	30105.90	.10254-01	.5203189

RESIDUAL STD DEV RESIDUAL D.F.
1.48848 161

* ESTIMATION OF B-SPLINE COEFFICIENTS *

I	B-SPLINE COEF	STD DEV
1	3711.5053	1.0525651
2	4153.7559	.41250259
3	10378.705	.41074148
4	12579.214	.57466792
5	13403.155	.74306913
6	14630.321	.62254084
7	16236.443	.41161732
8	22364.084	.44698178
9	22774.945	.43252287
10	27656.846	.39959609
11	30105.922	.52032419

<<<< GRID OF 300 EVENLY SPACED X VALUES CREATED >>>>
<<<< STD. DEV. OF 300 PREDICTED Y VALUES COMPUTED >>>>

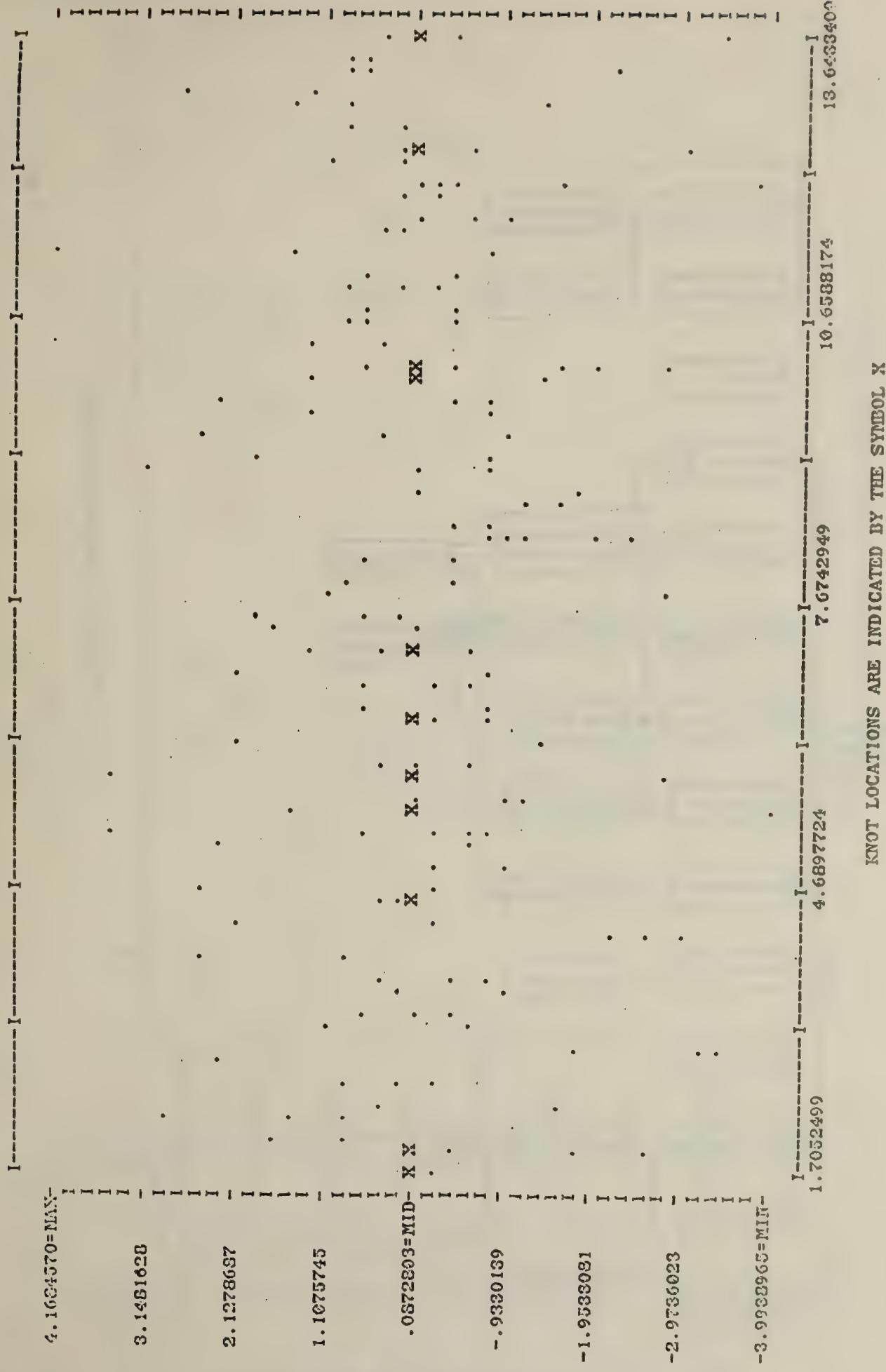
Figure 6. Regression fit.

* PIECEWISE POLYNOMIAL REPRESENTATION OF SPLINES *

..... INTERVAL			COEFFICIENTS OF $(X-X(I))^{**P}$		
I	X(I)	X(I+1)	P =	6	1
1	1.7052	1.8947		3711.5	2334.9
2	1.8947	4.5467		4153.8	2347.2
3	4.5467	5.4948		10379.	2321.0
4	5.4948	5.8738		12379.	2174.0
5	5.8738	6.4416		13403.	2161.5
6	6.4416	7.1899		14639.	2146.2
7	7.1899	10.043		16236.	2148.1
8	10.043	10.232		22364.	2168.6
9	10.232	12.504		22775.	2148.3
10	12.504	13.643		27657.	2150.4

Figure 7. Ordinary polynomial representation of the fitted spline.

Residuals (pascals) vs. independent variable (m^3).



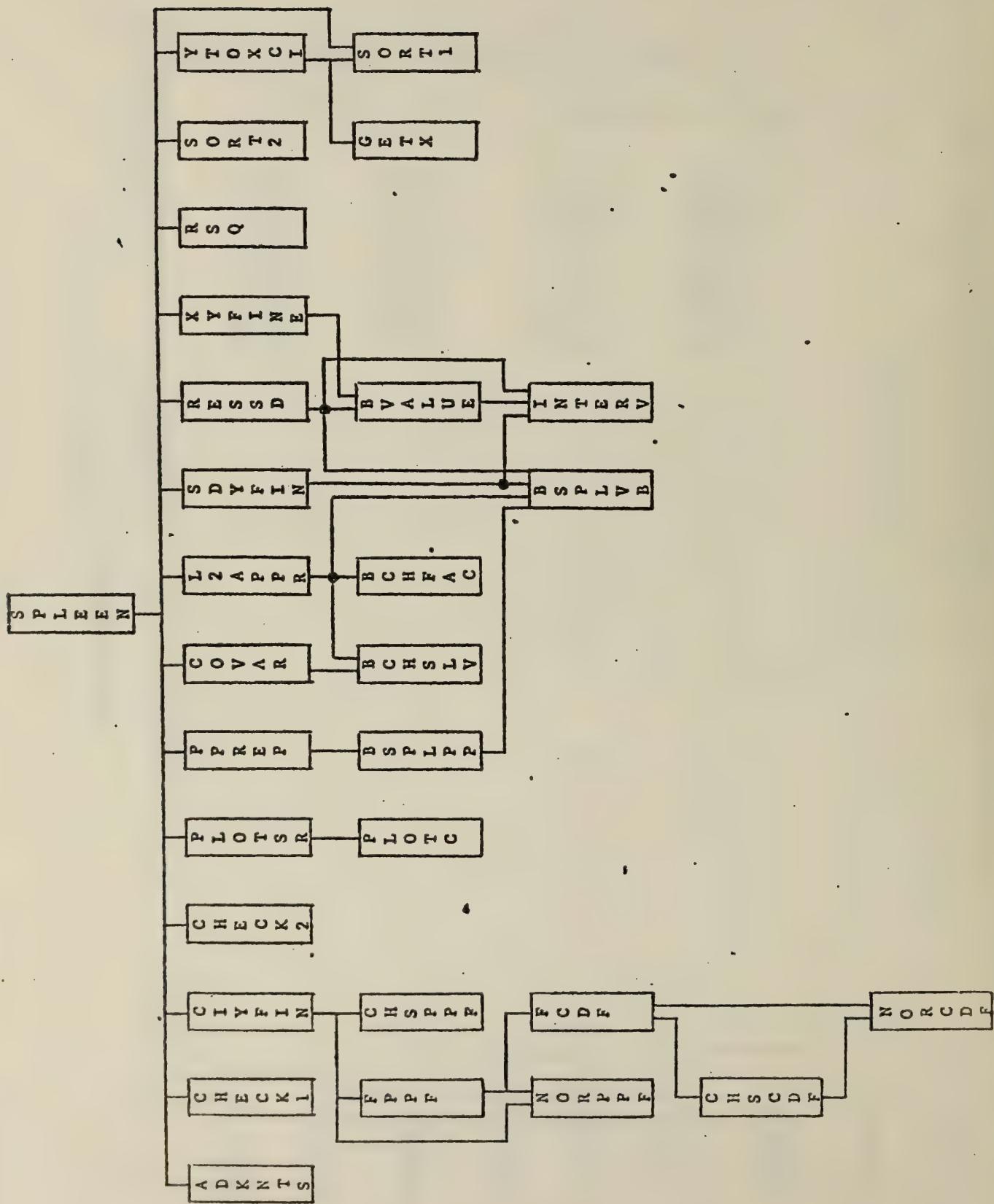


Figure 9. Diagram of subroutine interactions.

RESIDUALS VS. INDEPENDENT VARIABLE

3023.6694531=MAX-

2243.5394592

1467.3894653

689.2394714

-68.9195520=MID-

-867.0605469

-1645.2105103

-2423.3605347

-3201.5105591=MIN-

1.7052499

4.6897724

10.6588174

13.6433400

KNOT LOCATIONS ARE INDICATED BY THE SYMBOL, X

Figure 10: Diagnostic plot of residuals from a zero-degree spline fit (i.e., a step function).

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5. AUTHOR(S) James A. Lechner, Charles P. Reeve, Clifford H. Spiegelman						
6. PERFORMING ORGANIZATION (If joint or other than NBS, see instructions) NATIONAL BUREAU OF STANDARDS DEPARTMENT OF COMMERCE WASHINGTON, D.C. 20234				7. Contract/Grant No. 8. Type of Report & Period Covered		
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11. ABSTRACT (A 200-word or less factual summary of most significant information. If document includes a significant bibliography or literature survey, mention it here) <p>This paper presents a practical statistical overview of the pressure volume calibration curve for large nuclear materials processing tanks. It explains the appropriateness of applying splines (piecewise polynomials) to this curve, and it presents an overview of the associated statistical uncertainties. In order to implement these procedures a practical and portable FORTRAN IV program is provided along with its users' manual. Finally, the recommended procedure is demonstrated on actual tank data collected by NBS.</p>						
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